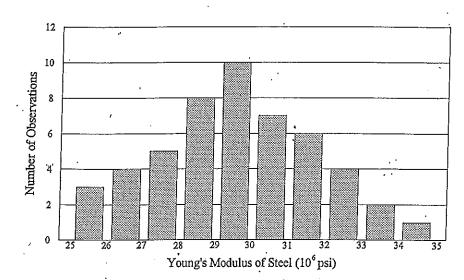
Solutions Manual

Singiresu S. Rao, Reliability Engineering, Pearson, Upper Saddle River, NJ, 2015

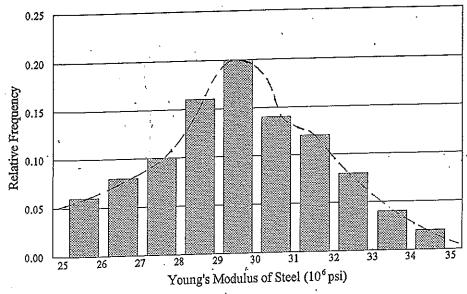
Chapter 1 Introduction

	,			:		•				
(1.1)	Data v			i			Interval	Observa	tions	Freq
	25.1	27.7	29.1	30.1	31.6		25-26	-,	3	0.060
10)	25.4	27.8	29.2	30,3	31.8		26-27	1	4	0.080
(a)	25.9	28.1	29.3	30.4	31,9		27-28	•	5	0.100
· /	26,5	28.3	29.4	30.5	32.3		28-29		8	0.160
	26.6	28.3	29,5	30.6	32.5		29-30 ·		10	0.200
	26.8	28.4	29.6	30.8	32.7		30-31		7	0.140
	26.9	28,5	29.6	30.9	32.8		31-32		6	0.120
	27.2	28.6	29.7	31.2	33.4		32-33		4	0.080
	27.4	28.7	29.8	31.3	33.8	•	33-34		2	0.040
	27.6	28.9	29.9	31,4	34.7		34-35		1	0.020
		,							50	1.000

Histogram







(c)

DATA !	YOUNG'S MOD	Xi - Xave	(Xi - Xave)^2
25.1	25100000	-4476000	
29.9	29900000	324000	
28.1			
32.5	32500000		8.5498E+12
28.5	28500000	-1076000	1.1578E+12
29.4	29400000	-176000	
25.4	25400000	-4176000	1.7439E+13
33.4	33400000	3824000	1.4623E+13
31.9	31900000		5.401E+12
26.6	26600000	-2976000	8.8566E+12
26.5	26500000	-3076000	
31.2	31200000	1624000	
29.2	29200000		1.4138E+11
26.9	26900000		7.161E+12
29.3	29300000		7.6176E+10
30.5	30500000		8.5378E+11
28.6	28600000	-976000	9.5258E+11
28.3	28300000		1.6282E+12
33.8	33800000		1.7842E+13
26.8	26800000	-2776000	7.7062E+12
27.4	27400000	-2176000	4.735E+12
32.3	32300000	2724000	7.4202E+12
29.8	29800000	224000	5.0176E+10
30.3	30300000		5.2418E+11
30.4	30400000	824000	
31.6	31600000	2024000	4.0966E+12
29.5	29500000	-76000	5776000000
28.7	28700000	-876000	7.6738E+11
30.9	309000001	1324000	1.753E+12

27.8	278000001	-1776000	3.1542E+12	
28.4	284000001	-1176000	1.383E+12	_
34.7	347.000001	5124000	2.6255E+13	
30.1	30100000	524000	2.7458E+11	
25.9	25900000	-3676000	1.3513E+13	
31.4	31400000	1824000	3.327E+12	_
32.8	. 32800000	3224000	1.0394E+13	_
30.6	30600000	1024000	1.0486E+12	_
29.6	296000001	24000	576000000	
29.6	29600000	24000	576000000	_
28.9	28900000	-676000	4.5698E+11	لـــا
29.1	29100000	-476000	2.2658E+11	
27.2	27200000	-2376000	5.6454E+12	
31.3	31300000	1724000	2.9722E+12	
27.6	27600000	-1976000	3.9046E+12	
32.7	32700000	3124000	9.7594E+12	_
28.3	28300000	-1276000	1.6282E+12	
31.8	31800000	2224000	4.9462E+12	
30.8	30800000	1224000	1.4982E+12	
27.7	27700000	-1876000	3.5194E+12	
29.7	29700000	124000	1.5376E+10	•
				_
TOTALSUM	1478800000	•	2.4079E+14	_
MEAN VALUE	29576000	4b/in2 -	•	_
STD DEV	2194498.58	Lb/in2		_
	,	. ,		_
			*	

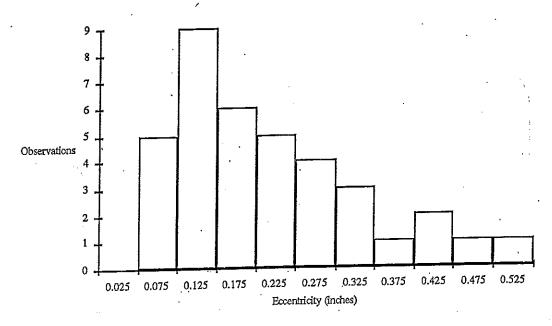
:. $\overline{X} = 29.5760$ Mpsi = mean value 8x = 2.1945 Mpsi = standard deviation

Observations of eccentricity of applied load

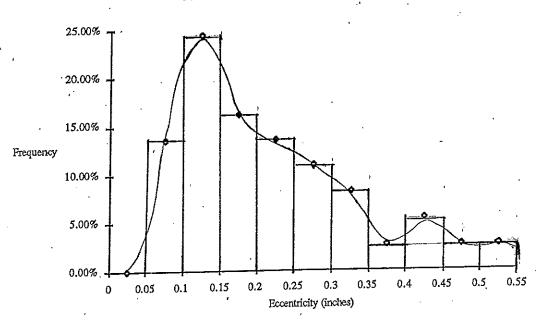
2 0.050 0.460 0.	
inches inches inches 1 0.410 0.410 0. 2 0.050 0.460 0.	1681 1706
1 0.410 0.410 0. 2 0.050 0.460 0.	1706
2 0.050 0.460 0.	1 .
one area a	1707
3 0.090 0.550 0.	
4 0.195 0.745 0.21	6725
5 0.345 1.090 0.3	3575
6 0.155 1.245 0.35	9775
7 0.320 1.565 0.46	2175
0.120 1.685 0.47	6575
9 0.290 1.975 0.56	0675
10 0.065 2.040 0.	5649
11 0.275 2.315 0.64	
12 0.230 2.545 0.693	
13 0.140 2.685 0.71	
14 0.265 2.950 0.76	8325
15 0.215 3.165 0.829	
16 0.070 3.235 0.834	4375
17 0.115 3.350 0.	8476
18 0.305 3.655 0.940	
19 0.435 4.090 1.13	2985
20 0.130 4,220 1.14	4675
21 0.535 4.755 1.43	2975
	5075
23 0.205 5.070 1.	4871
24 0.085 5.155 1.49	4325
25 0.135 5.290 1.5	1255
26 0.125 5.415 1.528	
27 0.185 5.600 1.5	5624
28 0.480 6.080 1.	7928
29 0.175 6.255 1.823	3425
30 0.145 6.400 1.84	4445
31 0.380 6.780 1.98	8885
32 0.165 6.945 2.016	
33 0.255 7.200 2.6	0811
34 0.180 7.380 2.	1135
35 0.240 7.620 2.	1711
36 0.220 7.840 2.3	2195
37 0.105 · 7.945 2.230	0525

٠.									1		
	Number	of obser	vations i	n each in	terval	1	•				
		0.05		0.15	0.2	0,25	0.3	0.35	0.4	0.45	0;5
From:	0.05		0.15	0.2	0.25	0,3	0.35	0.4	0.45	0.5	0.55
To:	0.05	0.1					0.325	0.375	0.425	0.475	0.525
Midpoint	0.025	0.075	0.125	0.175	0.220	0,510	0.010	1			1
Total:	0	5	9	6	5	4	3	1	E 4101	2.70%	2.70%
Traqueney.	0.00%	13.51%	24.32%	16.22%	13.51%	10.81%	8.11%	2.70%	5.41%	2.1070	2.7010

Column Load Eccentricity Histogram



Column Load Eccentricity Relative Frequency



Mean value of eccentricity =
$$\overline{E} = \frac{1}{N} \stackrel{N}{=} E_{i} = \frac{7.945}{37}$$

= 0.215 inch
Standard deviation of eccentricity = $\left\{\frac{1}{N} \stackrel{N}{=} \left(E_{i} - \overline{E}_{i}\right)^{2}\right\}^{\frac{1}{2}}$
= $\left\{\frac{1}{N} \stackrel{N}{=} E_{i}^{2} - \left(\frac{1}{N} \stackrel{N}{=} E_{i}\right)^{2}\right\}^{\frac{1}{2}} = 0.119$ inch

1.3) 29 values of maximum load carried by welded beams given.

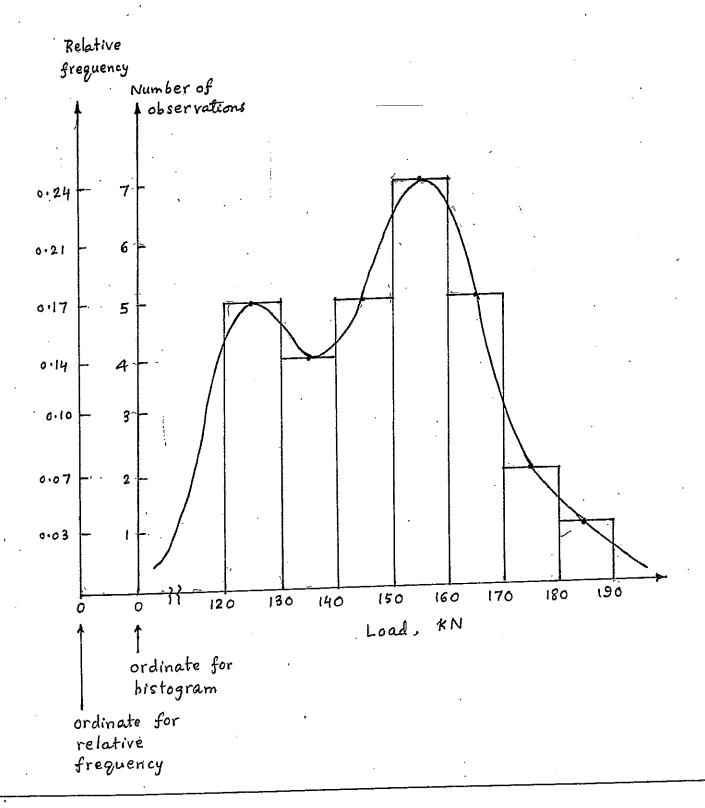
Smallest value: 123.1 KN, Largest value: 186.9 KN

Range chosen: 120 KNi - 190 KN

All data points are grouped into 7 intervals of 10 KN

each.

Range of load:	Frequency of load
	values falling in the range
2120 ≤ 130 KN	5
≥ 130 × 140 KN	4
2140 < 150 4N	5
2 150 < 160 KN	7
≥ 160 < 170 KN	5
= 170 < 180 KN	2
=180 <190 KN	1



1.4) Compressive strength of concrete cylinders, (in Kpsi):

Data: 32.2

5.9 6.2 5.8 7.8 6.5
$$\rightarrow$$
 Z = 32.2 6.3 8.9 5.3 3.7 1.4 \rightarrow Z = 25.6 2.1 6.8 9.1 4.3 3.2 \rightarrow Z = 25.5 7.2 6.1 5.7 4.9 2.6 \rightarrow Z = 26.5 3.4 6.8 8.3 5.1 7.3 \rightarrow Z = 30.9 8.2 7.7 5.4 3.7 4.5 \rightarrow Z = 29.5 4.1 5.6 6.4 6.7 7.9 \rightarrow Z = 30.7 6.9 7.5 5.2 4.3 6.6 \rightarrow Z = 30.5 5.4 6.4

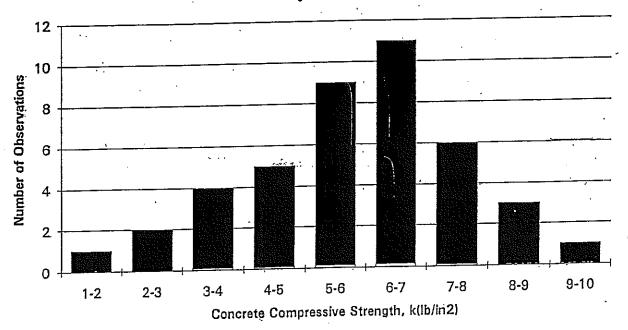
Total sum = 243.2

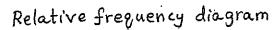
Mean value = $\overline{X} = \frac{243.2}{42} = 5.79$ Kpsi

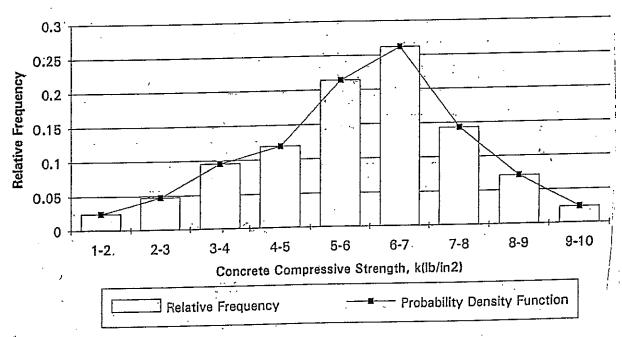
Standard deviation = $S_X = \left\{\frac{1}{N-1}\sum_{i=1}^{N} (X_i - \overline{X})^2\right\}^{\frac{1}{2}} = 1.81$ Kpsi

Range of compressive strength (KPSi)	Number of occurrances	Relative frequency
1 - 2	1	1/42 = 0.024
2-3	2 .	2/42 = 0.048
3-4	4	4/42 = 0.095
4-5	5	5/42 = 0.119
5-6	و	9/42 = 0.214
6-7	П.	11/42 = 0.262
7-8	6	6/42 = 0.143
8 — 9	3	3/42 = 0.071
9-10	1	1/42 = 0.024

Histogram







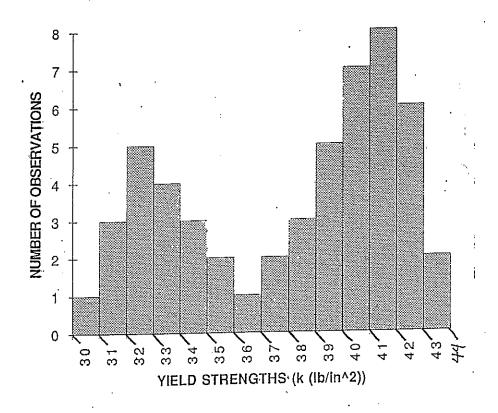
(1.5)

yield strength data of reinforcing bars (in Kpsi) made of two different grades of steel:

Range	# of Occourances	Relative Frequency
30,0 - 30,9	1	0.019
31.0 - 31.9	3	0.058
32.0 - 32.9	5	0.096
33,0 - 33,9	4	0.077
34.0 - 34.9	. 3	0.058
35,0 - 35,9	2	0.038
36.0 - 36.9	1	0.019
37.0 - 37.9	2	0,038
38.0 - 38.9	3	0.058
39,0 - 39,9	5	0.096
40.0 - 40.9	7	0.135
41.0 - 41.9	8	0.154
42.0 - 42.9	6	0.115
43.0 - 43.9	2	0.038

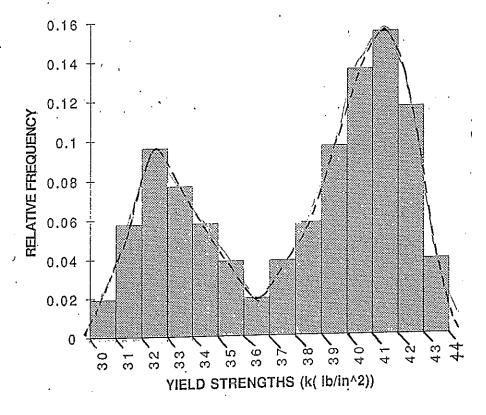
(a)

HISTOGRAM



(4)

RELATIVE FREQUENCY DIAGRAM,



(C) The relative frequency diagram has two distinct peaks which shows that the two grades of steel have two different average yield strengths which are approximately 32.5 and 41.5 k(lb/in²).

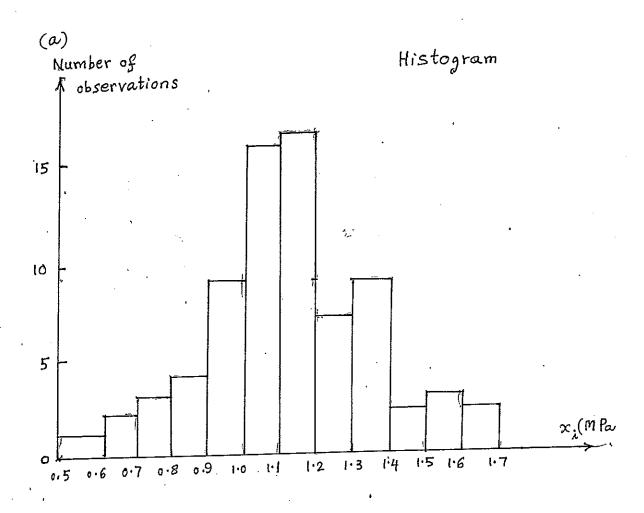
(d)

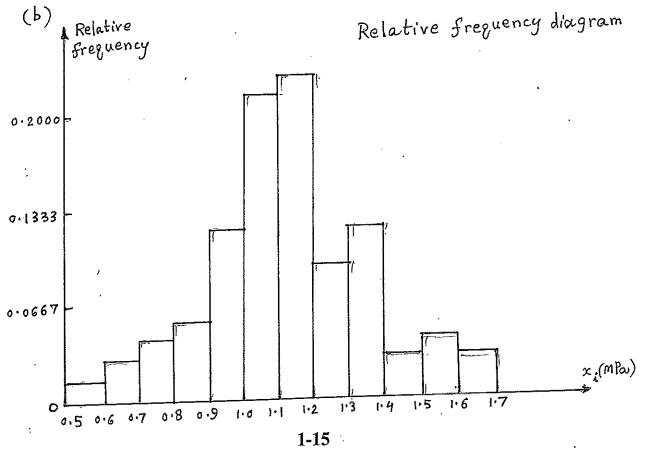
DATA Y.STRENGTHS XI - Xave (XI - Xave)^2 35.7 35700 -2315.38462 5361005.92 31.1 31100 -6915.38462 47822544.4 33.2 33200 -4815.38462 23187929 42.5 42500 4484.61538 20111775.1 41.2 41200 3184.61538 10141775.1 42.8 42800 4784.61538 22892544.4 37.5 37500 -515.384615 265621.302 40.7 40700 2684.61538 7207159.76 42.3 42300 4284.61538 18357929 42.2 42200 4184.61538 17511005.9 34.1 34100 -3915.38462 15330236.7 40.9 40900 2884.61538 8321005.92 43.3 43300 5284.61538 27927159.8 38.8 38800 784.615385 615621.302 40.9 40900 2884.61538 23859467.5 38.4 38400 384.61538 23859467.5			<u> </u>	
35.7 35700 -2315.38462 5361005.92 31.1 31100 -6915.38462 47822544.4 33.2 33200 -4815.38462 23187929 42.5 42500 4484.61538 20111775.1 41.2 41200 3184.61538 10141775.1 42.8 42800 4784.61538 22892544.4 37.5 37500 -515.384615 265621.302 40.7 40700 2684.61538 7207159.76 42.3 42300 4284.61538 18357929 42.2 42200 4184.61538 17511005.9 34.1 34100 -3915.38462 15330236.7 40.9 40900 2884.61538 3821005.92 43.3 43300 5284.61538 27927159.8 38.8 38800 784.615385 615621.302 40.9 40900 2884.61538 3230236.7 40.4 40400 2384.615385 147928.994 41.7 41700 3684.61538 13576390.5	DATA	Y, STRENGTHS	Xi - Xave	
33.2 33200 -4815.38462 23187929 42.5 42500 4484.61538 20111775.1 41.2 41200 3184.61538 10141775.1 42.8 42800 4784.61538 22892544.4 37.5 37500 -515.384615 265621.302 40.7 40700 2684.61538 7207159.76 42.3 42300 4284.61538 18357929 42.2 42200 4184.61538 17511005.9 34.1 34100 -3915.38462 15330236.7 40.9 40.900 2884.61538 321005.92 43.3 43300 5284.61538 321005.92 43.3 43300 5284.61538 321005.92 43.4 40.40 2384.61538 5686390.53 42.9 42.900 4884.61538 5686390.53 42.9 42.900 4884.61538 13576390.5 42.7 42700 4684.61538 13576390.5 42.7 42700 4684.61538 11455621.3 40.1 40100 2084.61538 11455621.3 41.4 41400 3384.61538 1403313.61 43.4 43400 5384.61538 1403313.61 43.4 43400 5384.61538 1403313.61 43.4 43400 5384.61538 28994082.8 39.6 39600 1584.61538 27954082.84 40.8 40.800 2784.61538 27954082.84 39.6 39600 1584.61538 27954082.84 39.6 39600 1584.61538 28994082.8 39.9 39900 1884.61538 26511005.92 33.8 33800 -4215.38462 2003313.61 39.9 39900 1884.61538 2651005.92 32.3 32300 -5715.38462 2003313.61 39.9 39900 1884.61538 2651005.92 32.9 32900 -5115.38462 2003313.61 32.3 32300 -5715.38462 2003313.61 32.3 32300 -5715.38462 20336390.5 32.9 32900 -5115.38462 20336390.5 34.5 34500 -3515.38462 17769467.5 36.6 36600 -1415.38462 2003313.61 39.9 39900 1884.61538 3551775.16 32.3 32300 -5715.38462 2003313.61 39.9 39900 1884.61538 3651775.16 32.3 32300 -5715.38462 2003313.61 39.9 39900 1884.61538 3651775.16 32.3 32300 -5715.38462 2003313.61 39.9 39900 -5115.38462 2003313.61		35700	-2315.38462	
42.5 42500 4484.61538 20111775.1 41.2 41200 3184.61538 10141775.1 42.8 42800 4784.61538 22892544.4 37.5 37500 -515.384615 265621.302 40.7 40700 2684.61538 7207159.76 42.3 42300 4284.61538 18357929 42.2 42200 4184.61538 17511005.9 34.1 34100 -3915.38462 15330236.7 40.9 40900 2884.61538 8321005.92 43.3 43300 5284.61538 27927159.8 38.8 38800 784.615385 615621.302 40.4 40400 2384.61538 23859467.5 38.4 38400 384.615385 147928.994 41.7 41700 3684.61538 13576390.5 42.7 42700 4684.61538 1345621.3 40.1 40100 2084.61538 1445621.3 41.4 41400 3384.61538 1403313.61 <t< td=""><td>31.1</td><td>31100</td><td>-6915.38462</td><td></td></t<>	31.1	31100	-6915.38462	
41.2 41200 3184.61538 10141775.1 42.8 42800 4784.61538 22892544.4 37.5 37600 -515.384615 265621.302 40.7 40700 2684.61538 7207159.76 42.3 42300 4284.61538 18357929 42.2 42200 4184.61538 17511005.9 34.1 34100 -3915.38462 15330236.7 40.9 40900 2884.61538 8321005.92 43.3 43300 5284.61538 27927159.8 38.8 38800 784.615385 615621.302 40.4 40400 2384.615385 666390.53 42.9 42900 4884.615385 147928.994 41.7 41700 3684.615385 147928.994 41.7 41700 3684.61538 21945621.3 40.1 40100 2084.61538 1455621.3 39.2 39200 1184.61538 1455621.3 40.8 4080 2784.61538 2511005.92 <	33.2	33200	-4815.38462	
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37.5 37500 -515.384615 265621.302 40.7 40700 2684.61538 7207159.76 42.3 42300 4284.61538 18357929 42.2 42200 4184.61538 17511005.9 34.1 34100 -3915.38462 15330236.7 40.9 40900 2884.61538 8321005.92 43.3 43300 5284.61538 27927159.8 38.8 38800 784.615385 615621.302 40.4 40400 2384.61538 5686390.53 42.9 42900 4884.61538 23859467.5 38.4 38400 384.61538 147928.994 41.7 41700 3684.61538 13576390.5 42.7 42700 4684.61538 21945621.3 40.1 40100 2084.61538 11455621.3 39.2 39200 1184.61538 11455621.3 40.8 4080 2784.61538 2511005.92 33.8 33800 -4215.38462 17769467.5 <	41,2	41200	3184.61538	L
37.5 37500 -515.384615 265621.302 40.7 .40700 2684.61538 7207159.76 42.3 42300 4284.61538 18357929 42.2 42200 4184.61538 17511005.9 34.1 34100 -3915.38462 15330236.7 40.9 40900 2884.61538 8321005.92 43.3 43300 5284.61538 27927159.8 38.8 38800 784.615385 615621.302 40.4 40400 2384.61538 5686390.53 42.9 42900 4884.61538 23859467.5 38.4 38400 384.61538 13576390.5 42.7 42700 4684.61538 13576390.5 42.7 42700 4684.61538 21945621.3 40.1 40100 2084.61538 4345621.3 41.4 41400 3384.61538 1455621.3 39.2 39200 1184.61538 1403313.61 43.4 43400 5384.61538 2894082.8 40.8 40800 2784.61538 2511005.92 33	42.8	42800	4784.61538	
42.3 42300 4284.61538 18357929 42.2 42200 4184.61538 17511005.9 34.1 34100 -3915.38462 15330236.7 40.9 40900 2884.61538 8321005.92 43.3 43300 5284.61538 27927159.8 38.8 38800 784.615385 615621.302 40.4 40400 2384.61538 5686390.53 42.9 42900 4884.61538 147928.994 41.7 41700 3684.61538 13576390.5 42.7 42700 4684.61538 21945621.3 40.1 40100 2084.61538 4345621.3 41.4 41400 3384.61538 1403313.61 43.4 43400 5384.61538 1403313.61 43.4 43400 5384.61538 2511005.92 33.8 33800 -4215.38462 17769467.5 36.6 36600 1584.61538 2511005.92 33.8 33800 -5715.38462 29326390.5			-515.384615	
42.2 42200 4184.61538 17511005.9 34.1 34100 -3915.38462 15330236.7 40.9 40900 2884.61538 8321005.92 43.3 43300 5284.61538 27927159.8 38.8 38800 784.615385 615621.302 40.4 40400 2384.61538 5686390.53 42.9 42900 4884.61538 147928.994 41.7 41700 3684.61538 13576390.5 42.7 42700 4684.61538 21945621.3 40.1 40100 2084.61538 4345621.3 41.4 41400 3384.61538 11455621.3 39.2 39200 1184.61538 1403313.61 43.4 43400 5384.61538 28994082.8 40.8 40800 2784.61538 2511005.92 33.8 33800 -4215.38462 17769467.5 36.6 36600 -1415.38462 2003313.61 39.9 39900 1884.61538 3551775.15	40.7	, 40700	2684.61538	7207159.76
34.1 34100 -3915.38462 15330236.7 40.9 40900 2884.61538 8321005.92 43.3 43300 5284.61538 27927159.8 38.8 38800 784.615385 615621.302 40.4 40400 2384.61538 5686390.53 42.9 42900 4884.61538 23859467.5 38.4 38400 384.615385 147928.994 41.7 41700 3684.61538 13576390.5 42.7 42700 4684.61538 21945621.3 40.1 40100 2084.61538 4345621.3 41.4 41400 3384.61538 1403313.61 39.2 39200 1184.61538 1403313.61 43.4 43400 5384.61538 28994082.8 40.8 40800 2784.61538 7754082.84 39.6 39600 1584.61538 2511005.92 33.8 33800 -4215.38462 17769467.5 36.6 36600 -1415.38462 2003313.61	42.3	42300	4284.61538	
40.9 40900 2884.61538 8321005.92 43.3 43300 5284.61538 27927159.8 38.8 38800 784.615385 615621.302 40.4 40400 2384.61538 5686390.53 42.9 42900 4884.61538 23859467.5 38.4 38400 384.615385 147928.994 41.7 41700 3684.61538 13576390.5 42.7 42700 4684.61538 21945621.3 40.1 40100 2084.61538 4345621.3 41.4 41400 3384.61538 1403313.61 39.2 39200 1184.61538 1403313.61 43.4 43400 5384.61538 2894082.8 39.6 39600 1584.61538 2511005.92 33.8 33800 -4215.38462 17769467.5 36.6 36600 -1415.38462 2003313.61 39.9 39900 1884.61538 3551775.15 32.3 32300 -5715.38462 29326390.5	42.2	42200	4184.61538	
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40.4 40400 2384.61538 5686390.53 42.9 42900 4884.61538 23859467.5 38.4 38400 384.615385 147928.994 41.7 41700 3684.61538 13576390.5 42.7 42700 4684.61538 21945621.3 40.1 40100 2084.61538 4345621.3 41.4 41400 3384.61538 1403313.61 43.4 43400 5384.61538 28994082.8 40.8 40800 2784.61538 7754082.84 39.6 39600 1584.61538 2511005.92 33.8 33800 -4215.38462 17769467.5 36.6 36600 -1415.38462 2003313.61 39.9 39900 1884.61538 3551775.15 32.3 32300 -5715.38462 32665621.3 32.9 32900 -5115.38462 29326390.5 32.9 32900 -5115.38462 29326390.5 32.9 32900 -515.38462 12357929 30.2 30200 -7815.38462 61080236.7	43.3	43300	5284.61538	
42.9 42900 4884.61538 23859467.5 38.4 38400 384.615385 147928.994 41.7 41700 3684.61538 13576390.5 42.7 42700 4684.61538 21945621.3 40.1 40100 2084.61538 4345621.3 41.4 41400 3384.61538 1403313.61 43.4 43400 5384.61538 28994082.8 40.8 40800 2784.61538 7754082.84 39.6 39600 1584.61538 2511005.92 33.8 33800 -4215.38462 17769467.5 32.3 32900 1884.61538 36551775.15 32.3 32300 -5715.38462 29326390.5 32.9 32900 -5115.38462 26167159.8 32.9 32900 -5115.38462 26167159.8 30.2 30200 -7815.38462 61080236.7 38.1 38100 84.61538 12142544.4 41.5 41500 3484.61538 12142544.4 31.2 31700 -6315.38462 39884082.8	38.8	38800	784.615385	
38.4 38400 384.615385 147928.994 41.7 41700 3684.61538 13576390.5 42.7 42700 4684.61538 21945621.3 40.1 40100 2084.61538 4345621.3 41.4 41400 3384.61538 1403313.61 43.4 43400 5384.61538 28994082.8 40.8 40800 2784.61538 7754082.84 39.6 39600 1584.61538 2511005.92 33.8 33800 -4215.38462 17769467.5 36.6 36600 -1415.38462 2003313.61 39.9 39900 1884.61538 3551775.15 32.3 32300 -5715.38462 29326390.5 32.9 32900 -5115.38462 26167159.8 30.2 32900 -5115.38462 12357929 30.2 30200 -7815.38462 12357929 30.1 38100 84.61538 12142544.4 41.5 41500 3484.61538 12142544.4 <	40.4	40400	2384.61538	
41.7 41700 3684.61538 13576390.5 42.7 42700 4684.61538 21945621.3 40.1 40100 2084.61538 4345621.3 41.4 41400 3384.61538 11455621.3 39.2 39200 1184.61538 1403313.61 43.4 43400 5384.61538 28994082.8 40.8 40800 2784.61538 7754082.84 39.6 39600 1584.61538 2511005.92 33.8 33800 -4215.38462 17769467.5 36.6 36600 -1415.38462 2003313.61 39.9 39900 1884.61538 3551775.15 32.3 32300 -5715.38462 29326390.5 32.9 32900 -5115.38462 29326390.5 32.9 32900 -5115.38462 22167159.8 34.5 34500 -3515.38462 12357929 30.2 30200 -7815.38462 61080236.7 38.1 38100 84.61538 12142544.4 41.5 41500 3484.61538 12142544.4 <	42.9	42900	4884.61538	<u> </u>
41.7 41700 3684.61538 13576390.5 42.7 42700 4684.61538 21945621.3 40.1 40100 2084.61538 4345621.3 41.4 41400 3384.61538 11455621.3 39.2 39200 1184.61538 1403313.61 43.4 43400 5384.61538 28994082.8 40.8 40800 2784.61538 7754082.84 39.6 39600 1584.61538 2511005.92 33.8 33800 -4215.38462 17769467.5 36.6 36600 -1415.38462 2003313.61 39.9 39900 1884.61538 3551775.15 32.3 32300 -5715.38462 32665621.3 32.9 32900 -5115.38462 29326390.5 32.9 32900 -5115.38462 12357929 30.2 30200 -7815.38462 12357929 30.1 38100 84.61538 12142544.4 41.5 41500 3484.61538 12142544.4 31.2 31200 -6815.38462 39884082.8 <td< td=""><td>38.4</td><td>38400</td><td>384.615385</td><td>147928.994</td></td<>	38.4	38400	384.615385	147928.994
42.7 42700 4684.61538 21945621.3 40.1 40100 2084.61538 4345621.3 41.4 41400 3384.61538 11455621.3 39.2 39200 1184.61538 1403313.61 43.4 43400 5384.61538 28994082.8 40.8 40800 2784.61538 7754082.84 39.6 39600 1584.61538 2511005.92 33.8 33800 -4215.38462 17769467.5 36.6 36600 -1415.38462 2003313.61 39.9 39900 1884.61538 3551775.15 32.3 32300 -5715.38462 32665621.3 32.6 32600 -5415.38462 29326390.5 32.9 32900 -5115.38462 226167159.8 34.5 34500 -3515.38462 12357929 30.2 30200 -7815.38462 61080236.7 38.1 38100 84.61538 12142544.4 41.5 41500 3484.61538 12142544.4 31.2 31200 -6815.38462 39884082.8			3684.61538	13576390.5
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39.6 39600 1584.61538 2511005.92 33.8 33800 -4215.38462 17769467.5 36.6 36600 -1415.38462 2003313.61 39.9 39900 1884.61538 3551775.15 32.3 32300 -5715.38462 32665621.3 32.6 32600 -5415.38462 29326390.5 32.9 32900 -5115.38462 26167159.8 34.5 34500 -3515.38462 12357929 30.2 30200 -7815.38462 61080236.7 38.1 38100 84.6153846 7159.76331 41.5 41500 3484.61538 12142544.4 31.2 31200 -6815.38462 46449467.5 31.7 31700 -6315.38462 39884082.8	43.4	43400	5384.61538	
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38.1 38100 84.6153846 7159.76331 41.5 41500 3484.61538 12142544.4 31.2 31200 -6815.38462 46449467.5 31.7 31700 -6315.38462 39884082.8 34.6 34600 -3415.38462 11664852.1	, 34.5			
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31.7 31700 -6315.38462 39884082.8 34.6 34600 -3415.38462 11664852.1	41.5			
34.6 34600 -3415.38462 11664852.1	31.2			
9,000	31.7			
41.1 41100 3084.61538 9514852.07				
	. 41.1	41100	3084.61538	9514852.07

37.2	37200	-815.384615	664852.071
39.5	39500		2204082.84
39.3	39300		1650236.69
35.5	35500	-2515.38462	6327159.76
33.7	33700		18622544.4
32.5			30419467.5
	40300	2284.615381	5219467.46
40.3	41800	3784.61538	14323313.6
41.8	32200	-5815.38462	33818698.2
32.2		2584.61538	6680236.69
140.6	40600	-4615.38462	21301775.1
33.4	33400	3584.61538	12849467.5
41.6	41600		10788698.2
41.3	.41300	3284.61538	10700030.2
			816187692
TOTAL SUM	1976800		810107032
MEAN VALUE	38015.3846		
STD. DEV.	3961.80731	LB/IN^2	
		<u> </u>	

Data on compressive strength of aluminum-lithium specimens (in MPa):

		······································
Interval of compressive strength (MPa)	Number of observed values	Relative frequency Value
0.5001-0.6000	1	0.0133
0.6001-0.7000	. 2	0.0267
0.7001-0.8000	3	0.04.00
0.8001-0.9000	4	0.05 33
0.9001 - 1.0000	9	0.1200
1.0001 - 1.1000	16	0.2133
1.1001 - 1.2000	17	0.2267
1.2001 - 1.3000	7	0.0933
1.3001 - 1.4000	9	0.1200
1.4001 - 1.5000	2	0.0267
1-5001 - 1.6000	3	0.0400
1.6001 - 1.7000	2	0.0267
Total	75	1.0000





(c) Mean value =
$$\bar{x} = \frac{1}{75} \sum_{i=1}^{75} x_i = \frac{1}{75} \left(1.0335 + 0.9302 + \dots + 1.3091 \right)$$

= 1.12.27 MPa

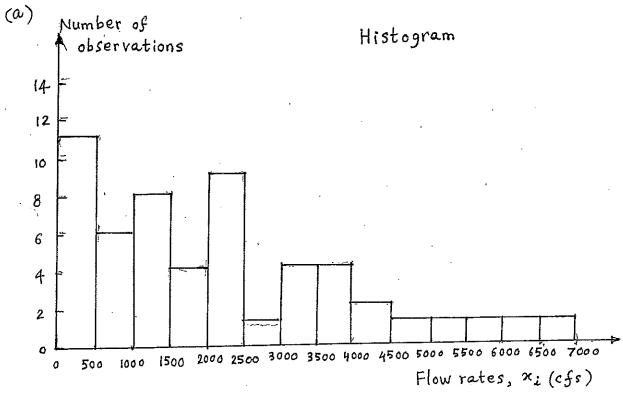
Standard deviation =
$$S_X = \left\{ \frac{1}{75} \sum_{i=1}^{75} (x_i - \overline{X})^2 \right\}^{\frac{1}{2}}$$

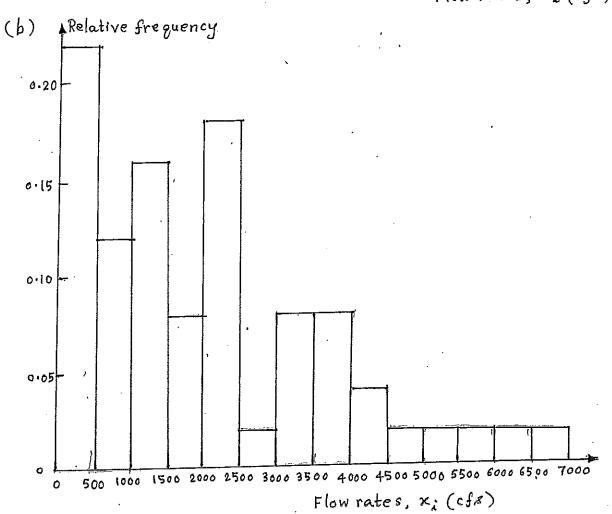
= $\left\{ \frac{1}{75} \left[(1.0335 - 1.1227)^2 + \dots + (1.3091 - 1.1227)^2 \right] \right\}^{\frac{1}{2}}$
= 0.0227 MPa

(d) From the given data, number of specimens that gave a value of x_i below 1 MPa = 19 out of $75 = \frac{19}{75} = 0.2533$ or 25.33%.

1.7) Data on annual flow rates in a river (in cfs): 50 data points:

Interval of flow rate (cf8)	Number of observed values	Relative frequency.
0 ~ 500	11	0.22
501-1000	6	0.12
1001 - 1500	8	0.16
1501 - 2000	4	0,08
2001 - 2500	9	0.18
2501 - 3000	1	0.02
3001 - 3500	4.	0.08
3501 - 4000	4	0.08
4001-4500	2	0.04
4501-5000	0	0
5001 - 5500	٥	0
5501 - 6000	O	ø
6001 - 6500	0	0
6501 - 7000	1, -	0.02
. Total	50	1.00





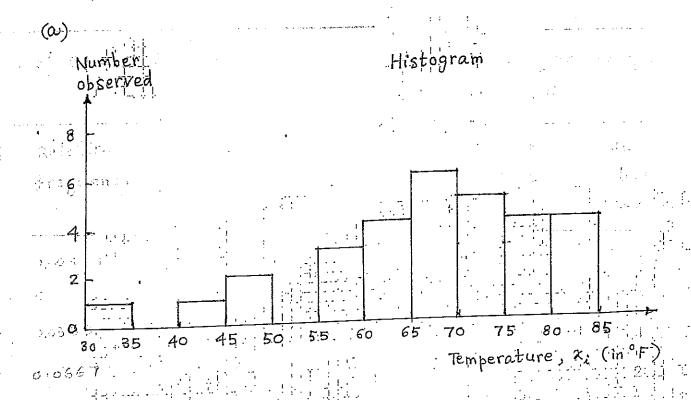
(c) Mean value =
$$\overline{X} = \frac{1}{50} \sum_{i=1}^{50} x_i = \frac{88579}{50}$$

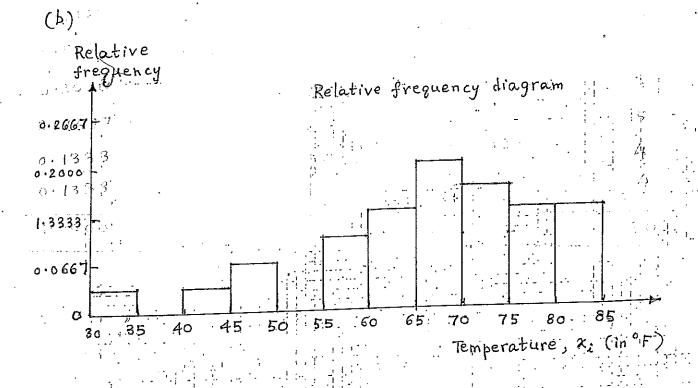
= 1,771.58 cfs
Standard deviation = $S_X = \left\{\frac{1}{50} \sum_{i=1}^{50} (x_i - 1771.58)^2\right\}^{\frac{1}{2}}$
= 1,382.9 cf8

(d) Percentage of flow notes exceeding as value of
$$4000 \text{ cfs} = 3 \text{ out of } 50 = 0.06$$
 or 6%

Data on joint temperatures of O-rings (in °F);
30 data points.

Interval of temperature	Number of observed values	Relative frequency
30-35	1	0.0333
35 - 40	0	O
40 - 45	i	0.03 3 3
45-50	2	0.0667
50 - 55	0	0
55-60	3	0.1000
60-65	4	0.1333
65-70	6	0.2000
70-75	j	0.1667
75 - 80	4	0.1333
80 - 85	4	0.1333
Total	30	1.0000





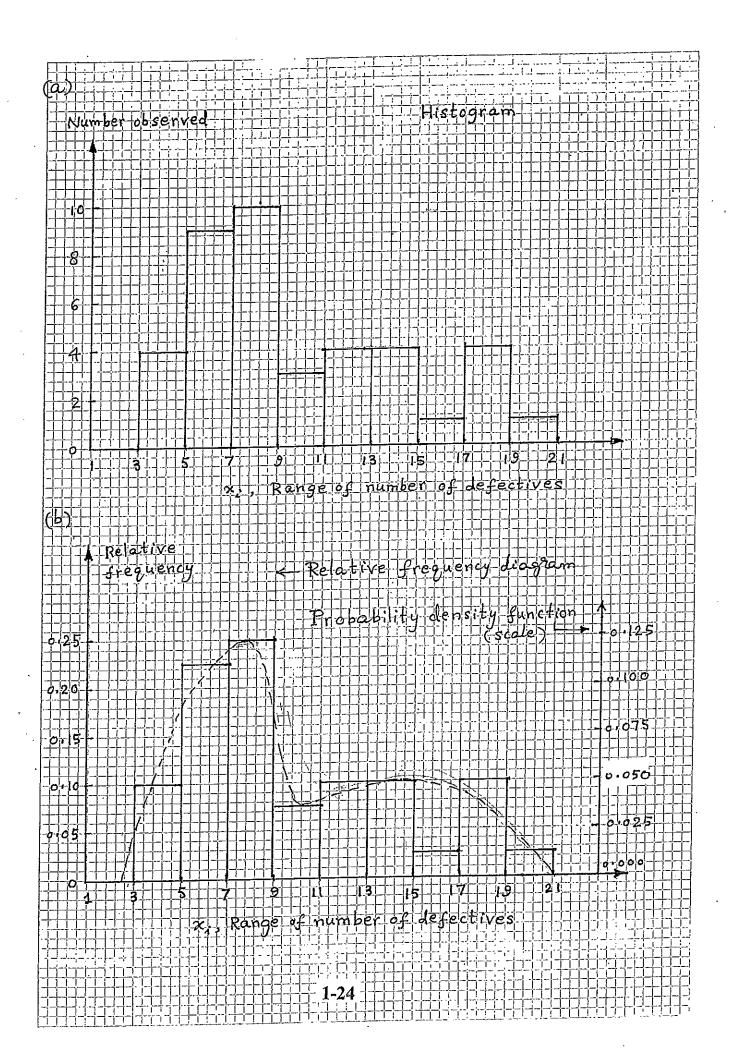
1.20

- (c) Mean value = $\overline{X} = \frac{1}{30} \stackrel{30}{\underset{i=1}{\text{Z}}} x_i = \frac{1976}{30} = 65.8667 \,^{\circ} F$ Standard deviation = $S_X = \left\{ \frac{1}{30} \stackrel{30}{\underset{i=1}{\text{Z}}} (x_i - 65.8667)^2 \right\}^{\frac{1}{2}}$ = $2.5498 \,^{\circ} F$
- (d) Percentage of joint temperatures falling below freezing point of water (32°F) is, from the observed data, o out of 30, i.e. 0%,

1.9 pata on number of dejective leaf springs in samples of size 50:

Total data points = 40

Range of number of defective springs	Number of observed values	Relative frequency
3 - 4.9	4	0.100
5 - 6.9	9	0.225
7 - 8.9	.10	0.250
9-10.9	3	0.075
11 - 12.9	. 4	0.100
13 - 14.9	4	0.100
15 - 16.9	t	0.025
17 - 18.9	.4	0.100
19-20.9	11	0.025
Total:	40	1.000



(c) Mean value =
$$\bar{X} = \frac{1}{40} \sum_{i=1}^{40} x_i = 9.375$$

Standard deviation = $l_X = \left\{ \frac{1}{40} \sum_{i=1}^{40} (x_i - 9.375)^2 \right\}^{\frac{1}{2}}$
= 4.4761

(d) Percentage of defective springs that fall outside the band defined by (mean ± 3 standard deviations)

i.e., 9.375 ± 3 (4.4761) = 9.375 ± 13.4283

i.e., -4.0533 to 22.8033

i.e., o to 22.8033

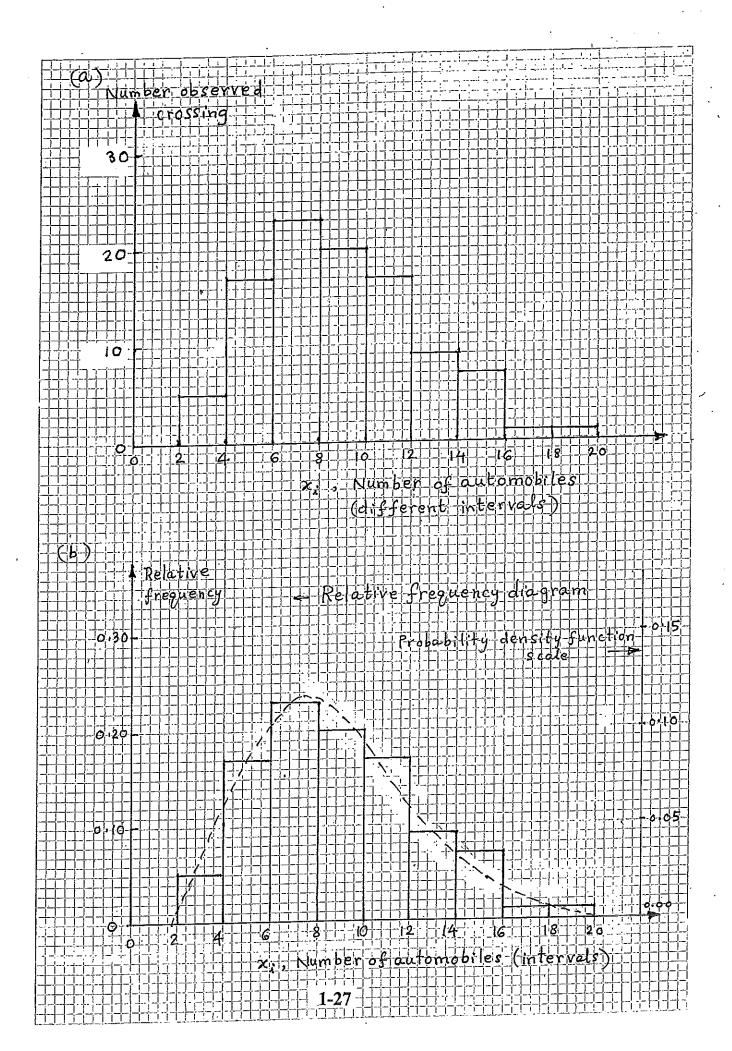
From the given data, we find that none of the data falls outside o-22.8033

Hence the required percentage is zero.

1.10 Data on number of automobiles crossing an intersection:

Data points: 100

Numbe	r	Number	Relative
of automo	biles	ob served	frequency
crossir interse			
1		O	` Ø
2		0	Ø
3		2 -	0.02
4	•	3	0.03
5		7	0.07
6		10 -	0.10
7		. H	0.11
8	:	12	0.12
9	}	14	0.14
10	į.	6	0.06
11		7	0.07
12	,	10	0.10
(3		6`	0.06
14		3	0.03
15		. 6	0.06
16		· I	0.01
17	•	1	0.01
18	٠.,	0	. О
19		ĺ	0.01
20		O	0
,	Total:	100	1.00

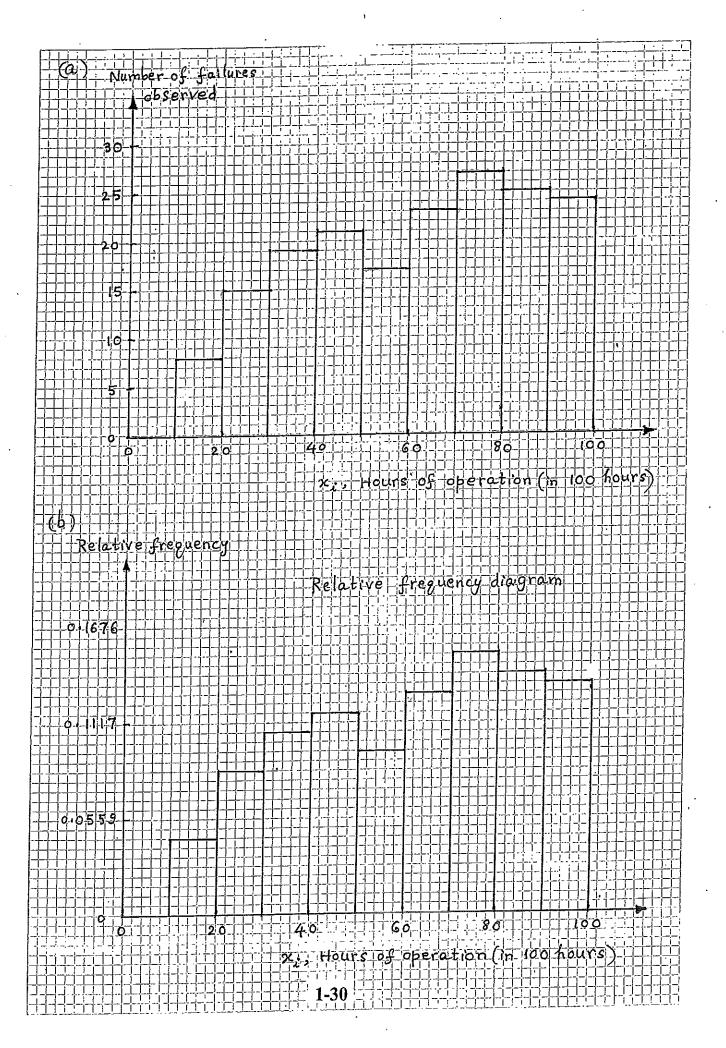


- (c) Sample mean = $\frac{1}{100} \sum_{i=1}^{100} x_i = 9.31 = \overline{X}$ Sample standard deviation = $\left\{ \frac{1}{99} \sum_{i=1}^{100} (x_i - 9.31)^2 \right\}^{\frac{1}{2}}$ = $S_X = 3.3795$
- (d) Percentage of number of automobiles exceeding a value of 15 (from given data) is 3 out of 100, i.e., 3%.

(1.11)

Failure data of disk drives: Total number of failures: 179

Hours of operation (unit: 100 hours)	Number of failures observed	Relative frequency
0 - 10.0	O	ø
10.1- 20.0	8	0.0447
20.1-30.0	15	0.0838
30.1-40.0	19	0.1061
40.1 - 50.0	21	0.1173
50.1 - 60.0	17	0.0950
60:1 - 70:0	23	0.1285
70.1-80.0	27	0.1508
80.1- 90.0	25	0.1397
90.1-100.0	24	0.1341
Total:	179	[.0000



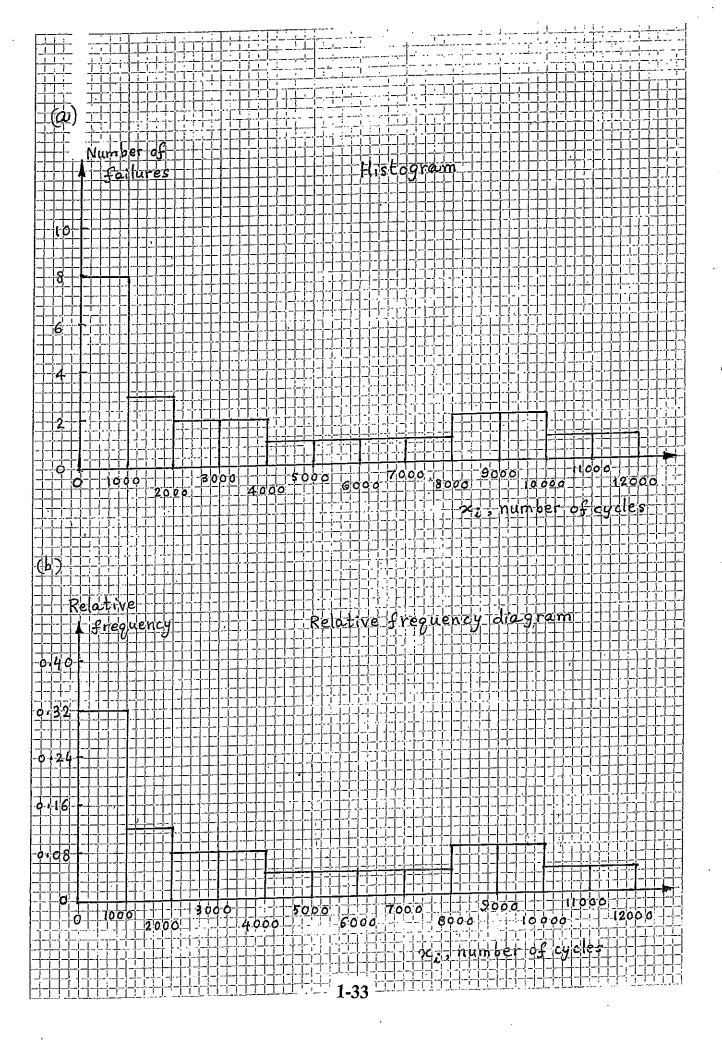
- (c) Sample mean = $\bar{x} = \left(\frac{1}{179} \sum_{i} x_{i}\right) = 61.257 \times 100 \text{ hours}$ Sample standard deviation = $8x = 23.99 \times 100 \text{ hours}$
- (d) Expected reliability of disk drives at 8,000 hours of operation (from given data)
 - = Probability of hours of operation > 80 units
 - = (25+24) out of 179 failures
 - = 0.2737

(1.12)

Failure data of turbine blades

Data points: 25

Number of cycles at failure (Range)	Number of failwies observed in the range	Relative frequency
0 - 1000.	8	0.32
1001 - 2000	3	0.12
2001 - 3000	2	. 0.08
3001-4000	2	0.08
4001 - 5000	ı	0.04
5001-6000	ı I	0.04
6001-7000	1,	0.04
7001 - 8000		0.04
8001-9000	2	0.08
9001 - 10000	2	0.08
10001 - 11000	1	0.04
11001 - 12000	1 .	0.04
Total:	2.5	1.00



- (c) Sample mean = $\overline{X} = \frac{1}{25} \sum_{i=1}^{25} x_i = 4125.16$ cycles Sample standard deviation = $8x = \left\{\frac{1}{25} \sum_{i=1}^{25} (x_i - \overline{X})^2\right\}^{\frac{1}{2}}$ = 3765.42 cycles
 - (d) Percentage of turbine blades that have a life greater than 7500 cycles (from given data)
 = 7 out of 25 = 28%.