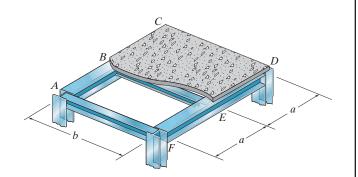
2–1. The steel framework is used to support the reinforced stone concrete slab that is used for an office. The slab is 200 mm thick. Sketch the loading that acts along members BE and FED. Take a=2 m, b=5 m. Hint: See Tables 1.2 and 1.4.



SOLUTION

Beam BE. Since $\frac{b}{a} = \frac{5 \text{ m}}{2 \text{ m}} = 2.5$, the concrete slab will behave as a one-way slab.

Thus, the tributary area for this beam is rectangular, as shown in Fig. a, and the intensity of the uniform distributed load is

200 mm thick reinforced stone concrete slab:

$$(23.6 \text{ kN/m}^3)(0.2 \text{ m})(2 \text{ m}) = 9.44 \text{ kN/m}$$

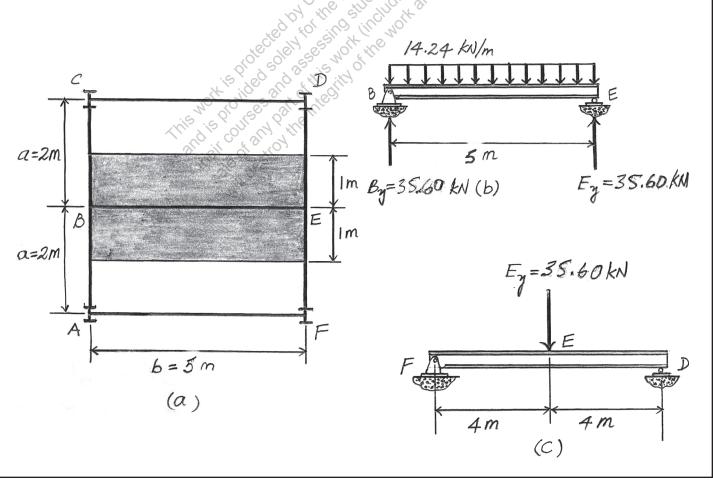
Live load for office: $(2.40 \text{ kN/m}^2)(2 \text{ m}) = 4.80 \text{ kN/m}$

Due to symmetry the vertical reactions at B and E are

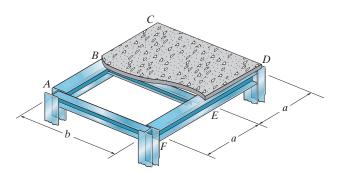
$$B_v = E_v = (14.24 \text{ kN/m})(5)/2 = 35.6 \text{ kN}$$

The loading diagram for beam BE is shown in Fig. b.

Beam FED. The only load this beam supports is the vertical reaction of beam BE at E, which is $E_v = 35.6$ kN. The loading diagram for this beam is shown in Fig. c.



2–2. Solve Prob. 2–1 with a = 3 m, b = 4 m.



SOLUTION

Beam BE. Since $\frac{b}{a} = \frac{4}{3} < 2$, the concrete slab will behave as a two-way slab. Thus,

the tributary area for this beam is the hexagonal area shown in Fig. a, and the maximum intensity of the distributed load is

200 mm thick reinforced stone concrete slab: $(23.6 \text{ kN/m}^3)(0.2 \text{ m})(3 \text{ m})$ = 14.16 kN/m

Live load for office:
$$[(2.40 \text{ kN/m}^2)(3 \text{ m})] = 7.20 \text{ kN/m}$$

21.36 kN/m

Due to symmetry, the vertical reactions at B and E are

$$B_y = E_y = \frac{2\left[\frac{1}{2}(21.36 \text{ kN/m})(1.5 \text{ m})\right] + (21.36 \text{ kN/m})(1 \text{ m})}{2}$$
= 26.70 kN

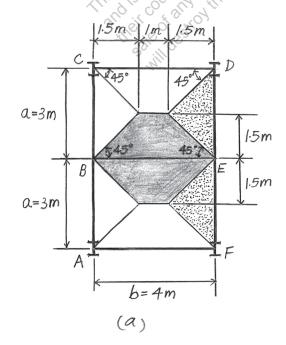
The loading diagram for beam BE is shown in Fig. b.

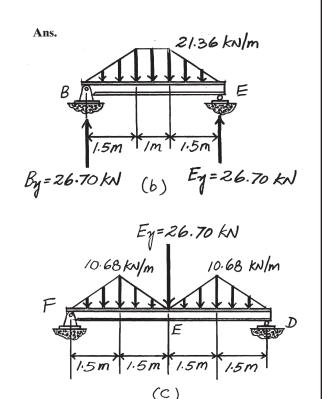
Beam FED. The loadings that are supported by this beam are the vertical reaction of beam BE at E which is $E_y=26.70$ kN and the triangular distributed load of which its tributary area is the triangular area shown in Fig. a. Its maximum intensity is

200 mm thick reinforced stone concrete slab: $(23.6 \text{ kN/m}^3)(0.2 \text{ m})(1.5 \text{ m})$ = 7.08 kN/m

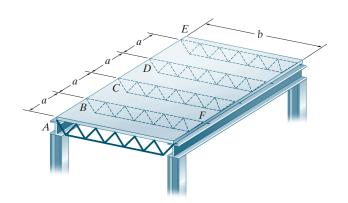
Live load for office: $(2.40 \text{ kN/m}^2)(1.5 \text{ m}) = \frac{3.60 \text{ kN/m}}{10.68 \text{ kN/n}}$

The loading diagram for beam FED is shown in Fig. c.





2–3. The floor system used in a school classroom consists of a 4-in. reinforced stone concrete slab. Sketch the loading that acts along the joist BF and side girder ABCDE. Set a = 10 ft, b = 30 ft. *Hint:* See Tables 1.2 and 1.4.



SOLUTION

Joist BF. Since $\frac{b}{a} = \frac{30 \text{ ft}}{10 \text{ ft}} = 3$, the concrete slab will behave as a one-way slab.

Thus, the tributary area for this joist is the rectangular area shown in Fig. a, and the intensity of the uniform distributed load is

4-in.-thick reinforced stone concrete slab: $(0.15 \text{ k/ft}^3) \left(\frac{4}{12} \text{ ft}\right) (10 \text{ ft}) = 0.5 \text{ k/ft}$

Live load for classroom: $(0.04 \text{ k/ft}^2)(10 \text{ ft})$

$$= 0.4 \, k/ft$$

Ans.

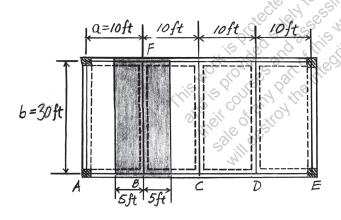
Due to symmetry, the vertical reactions at B and F are

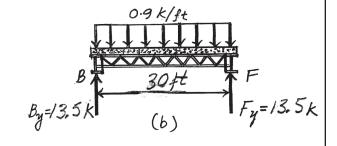
$$B_v = F_v = (0.9 \text{ k/ft})(30 \text{ ft})/2 = 13.5 \text{ k}$$

Ans

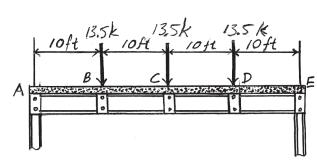
The loading diagram for joist BF is shown in Fig. b.

Girder ABCDE. The loads that act on this girder are the vertical reactions of the joists at B, C, and D, which are $B_y = C_y = D_y = 13.5$ k. The loading diagram for this girder is shown in Fig. c.



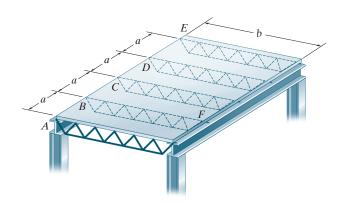


(a)



(c)

*2-4. Solve Prob. 2-3 with a = 10 ft, b = 15 ft.



SOLUTION

Joist BF. Since $\frac{b}{a} = \frac{15 \text{ ft}}{10 \text{ ft}} = 1.5 < 2$, the concrete slab will behave as a two-way slab. Thus, the tributary area for the joist is the hexagonal area, as shown in Fig. a, and the maximum intensity of the distributed load is

4-in.-thick reinforced stone concrete slab: $(0.15 \text{ k/ft}^3) \left(\frac{4}{12} \text{ ft}\right) (10 \text{ ft}) = 0.5 \text{ k/ft}$

Live load for classroom: $(0.04 \text{ k/ft}^2)(10 \text{ ft})$

Due to symmetry, the vertical reactions at B and G are

ad for classroom:
$$(0.04 \text{ k/ft}^2)(10 \text{ ft})$$
 = 0.4 k/ft
 0.9 k/ft
Ans. symmetry, the vertical reactions at B and G are
$$B_y = F_y = \frac{2\left[\frac{1}{2}(0.9 \text{ k/ft})(5 \text{ ft})\right] + (0.9 \text{ k/ft})(5 \text{ ft})}{2} = 4.50 \text{ k}$$
 Ans. adding diagram for beam BF is shown in Fig. B .

ABCDE. The loadings that are supported by this girder are the vertical ns of the joist at B , C and D , which are $B_y = C_y = D_y = 4.50 \text{ k}$, and the lar distributed load shown in Fig. a . Its maximum intensity is nick reinforced stone concrete slab:

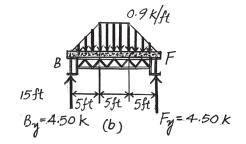
The loading diagram for beam BF is shown in Fig. b,

Girder ABCDE. The loadings that are supported by this girder are the vertical reactions of the joist at B, C and D, which are $B_y = C_y = D_y = 4.50$ k, and the triangular distributed load shown in Fig. a. Its maximum intensity is

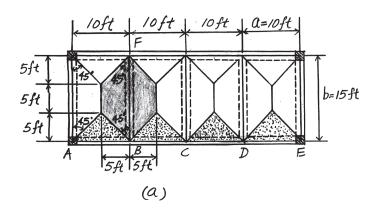
4-in.-thick reinforced stone concrete slab:

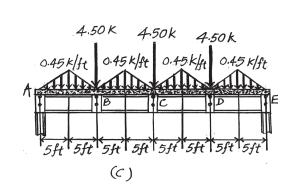
$$(0.15 \,\mathrm{k/ft^3}) \left(\frac{4}{12} \,\mathrm{ft}\right) (5 \,\mathrm{ft}) = 0.25 \,\mathrm{k/ft}$$

Live load for classroom: (0.04 k/ft²)(5 ft)

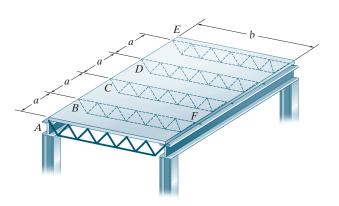


The loading diagram for the girder ABCDE is shown in Fig. c.





2–5. Solve Prob. 2–3 with a = 7.5 ft, b = 20 ft.

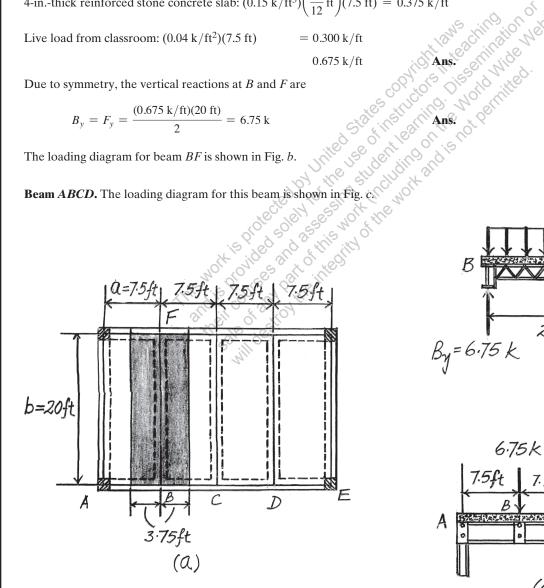


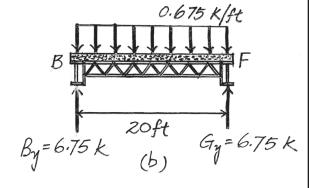
SOLUTION

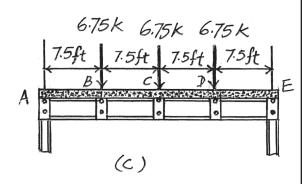
Beam BF. Since $\frac{b}{a} = \frac{20 \text{ ft}}{7.5 \text{ ft}} = 2.7 > 2$, the concrete slab will behave as a one-way slab. Thus, the tributary area for this beam is a rectangle, as shown in Fig. a, and the intensity of the distributed load is

4-in.-thick reinforced stone concrete slab: $(0.15 \text{ k/ft}^3) \left(\frac{4}{12} \text{ ft}\right) (7.5 \text{ ft}) = 0.375 \text{ k/ft}$

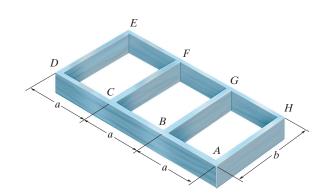
$$B_y = F_y = \frac{(0.675 \text{ k/ft})(20 \text{ ft})}{2} = 6.75 \text{ k}$$







2–6. The frame is used to support a 2-in.-thick plywood floor of a residential dwelling. Sketch the loading that acts along members BG and ABCD. Set a=6 ft, b=18 ft. *Hint:* See Tables 1.2 and 1.4.



SOLUTION

Beam BG. Since $\frac{b}{a} = \frac{18 \text{ ft}}{6 \text{ ft}} = 3 > 2$, the plywood platform will behave as one-way

slab. Thus, the tributary area for the beam is rectangular and shown shaded in Fig. a. The intensity of the uniform distributed load is

2-in.-thick plywood platform:
$$\left(36 \frac{lb}{ft^3}\right) \left(\frac{2}{12} \text{ ft}\right) (6 \text{ ft}) = 36 \text{ lb/ft}$$

Live load for residential dwelling:
$$\left(40 \frac{\text{lb}}{\text{ft}^2}\right) (6 \text{ ft}) = \frac{240 \text{ lb/ft}}{276 \text{ lb/ft}}$$

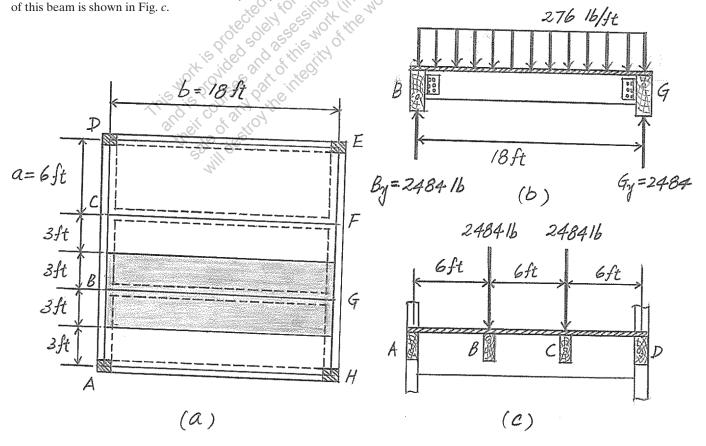
Due to symmetry, the vertical reaction at B and G are

The loading diagram for beam BG is shown in Fig. b.

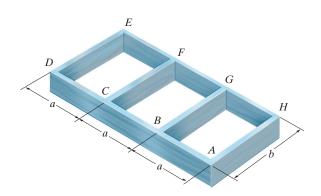
$$B_y = G_y = \frac{(276 \text{ lb/ft})(18 \text{ ft})}{2} = 2484 \text{ lb}$$

Staring Mil

Beam ABCD. The loads that act on this beam are the vertical reaction of beams BG and CF at B and C respectively, which are $C_y = B_y = 2484$ lb. The loading diagram



2–7. Solve Prob. 2–6, with a = 10 ft, b = 10 ft.



SOLUTION

Beam BG. Since $\frac{b}{a} = \frac{10 \text{ ft}}{10 \text{ ft}} = 1 < 2$, the plywood platform will behave as a two-way

slab. Thus, the tributary area for this beam is the shaded square area shown in Fig. a, and the maximum intensity of the triangular distributed load is

2-in.-thick plywood platform: $\left(36 \frac{\text{lb}}{\text{ft}^3}\right) \left(\frac{2}{12} \text{ ft}\right) (10 \text{ ft}) = 60 \text{ lb/ft}$

Live load for residential dwelling: $\left(40 \frac{\text{lb}}{\text{ft}^2}\right) (10 \text{ ft}) = \frac{400 \text{ lb/ft}}{460 \text{ lb/ft}}$

Due to symmetry, the vertical reaction at B and G are

$$B_y = G_y = \frac{\frac{1}{2} (460 \text{ lb/ft})(10 \text{ ft})}{2} = 1150 \text{ lb}$$

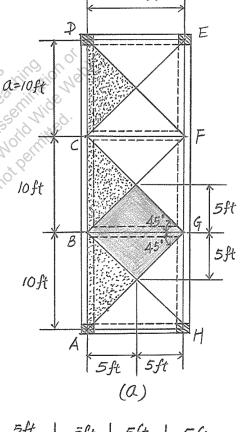
The loading diagram for beam BG is shown in Fig. b.

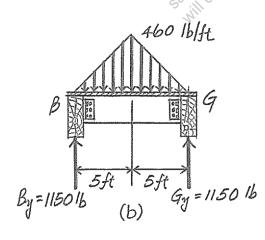
Beam *ABCD*. The loadings that are supported by this beam are the vertical reaction of beams BG and CF at B and C respectively, which are $B_y = C_y = 1150$ lb and the triangular distributed load contributed by the dotted triangular area shown in Fig. a. Its maximum intensity is

2-in.-thick plywood platform:
$$\left(36\frac{lb}{ft^3}\right)\left(\frac{2}{12}ft\right)(5ft) = 30 lb/ft$$

Live load for residential dwelling: $\left(40 \frac{\text{lb}}{\text{ft}^2}\right) (5 \text{ ft}) = \frac{200 \text{ lb/ft}}{230 \text{ lb/ft}}$ Ans.

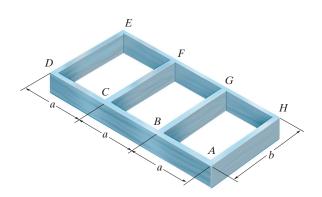
The loading diagram for beam ABCD is shown in Fig. c.





Beam *ABCD***.** 1150 lb at *B* and *C*, $w_{\text{max}} = 230 \text{ lb/ft}$

*2-8. Solve Prob. 2-6, with a = 10 ft, b = 15 ft.



SOLUTION

Beam BG. Since $\frac{b}{a} = \frac{15 \text{ ft}}{10 \text{ ft}} = 1.5 < 2$, the plywood platform will behave as a two-way

slab. Thus, the tributary area for this beam is the shaded octagonal area shown in Fig. a, and the maximum intensity of the trapezoidal distributed load is

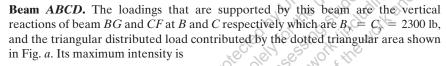
2-in.-thick plywood platform: $\left(36 \frac{\text{lb}}{\text{ft}^3}\right) \left(\frac{2}{12} \text{ ft}\right) (10 \text{ ft}) = 60 \text{ lb/ft}$

Live load for residential dwelling: $\left(40 \frac{lb}{ft^2}\right) (10 \text{ ft}) = \frac{400 \text{ lb/ft}}{460 \text{ lb/ft}}$

Due to symmetry, the vertical reactions of B and G are

symmetry, the vertical reactions of
$$B$$
 and G are
$$B_y = G_y = \frac{\frac{1}{2} (460 \text{ lb/ft})(15 \text{ ft} + 5 \text{ ft})}{2} = 2300 \text{ lb}$$
ding diagram for beam BG is shown in Fig. b .

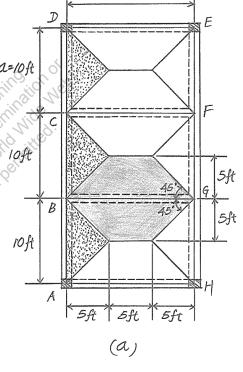
The loading diagram for beam BG is shown in Fig. b.



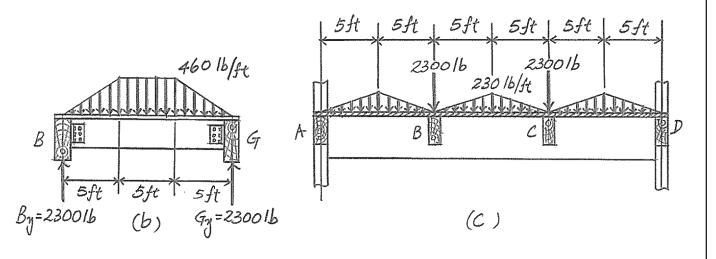
2-in.-thick plywood platform: $(36 lb/ft^3) \left(\frac{2}{12} ft\right) (5 ft) = 30 lb/ft$

Live load for residential dwelling: $(40 \text{ lb/ft}^2)(5 \text{ ft}) = \frac{200 \text{ lb/ft}}{230 \text{ lb/ft}}$

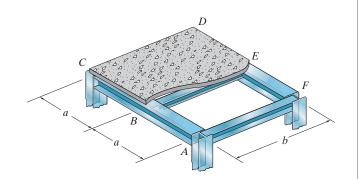
The loading diagram for beam ABCD is shown in Fig. c.



b=15ft



2–9. The steel framework is used to support the 4-in. reinforced stone concrete slab that carries a uniform live loading of 400 lb/ft^2 . Sketch the loading that acts along members BE and FED. Set a = 9 ft, b = 12 ft. *Hint:* See Table 1.2.



SOLUTION

Beam BE. Since $\frac{b}{a} = \frac{12 \text{ ft}}{9 \text{ ft}} = \frac{4}{3} < 2$, the concrete slab will behave as a two-way

slab. Thus, the tributary area for this beam is the shaded octagonal area shown in Fig. a, and the maximum intensity of the trapezoidal distributed load is

4-in.-thick reinforced stone concrete slab: $(0.15 \text{ k/ft}^3) \left(\frac{4}{12} \text{ ft}\right) (9 \text{ ft}) = 0.45 \text{ k/ft}$

Floor live load:
$$(0.4 \text{ k/ft}^2)(9 \text{ ft})$$
 = $\frac{3.60 \text{ k}}{4.05 \text{ k}}$

Ans

Due to symmetry, the vertical reactions at B and E are

$$B_y = E_y = \frac{\frac{1}{2} (4.05 \text{ k/ft})(3 \text{ ft} + 12 \text{ ft})}{2} = 15.19 \text{ k}$$

Ans.

The loading diagram of beam BE is shown in Fig. a.

Beam FED. The loadings that are supported by this beam are the vertical reactions of beam BE at E, which is $E_y=15.19\,\mathrm{k}$ and the triangular distributed load contributed by dotted triangular tributary area shown in Fig. a. Its maximum intensity is

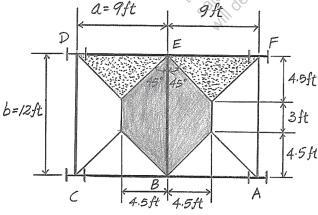
4-in.-thick concrete slab: $(0.15 \text{ k/ft}^3) \left(\frac{4}{12} \text{ ft}\right) (4.5 \text{ ft}) = 0.225 \text{ k/ft}$

Floor live load: $(0.4 \text{ k/ft}^2)(4.5 \text{ ft})$ = $\frac{1.800 \text{ k/f}}{2.025 \text{ k/f}}$

Ans. $B_{y} = 15.19 k$ $E_{y} = 15.19 k$ (b)

4.05 K/ft

The loading diagram of beam FED is shown in Fig. c.



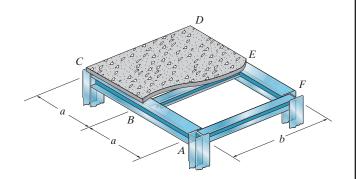
(a)

D E 2.025 k/st 4.5ft 4.5ft 4.5ft 4.5ft

Beam *BE*. $w_{\text{max}} = 4.05 \text{ k/ft}$

Beam FED. 15.2 k at E, $w_{\text{max}} = 2.025 \text{ k/ft}$

2–10. Solve Prob. 2–9, with a = 6 ft, b = 18 ft.



SOLUTION

Beam BE. Since $\frac{b}{a} = \frac{18 \text{ ft}}{6 \text{ ft}} = 3 > 2$, the concrete slab will behave as a one-way slab. Thus, the tributary area for this beam is the shaded rectangular area shown in Fig. a, and the intensity of the uniform distributed load is

4-in.-thick reinforced stone concrete slab: $(0.15 \, k/ft^3) \left(\frac{4}{12} \, ft\right) (6 \, ft) = 0.30 \, k/ft$

Floor live load:
$$(0.4 \text{ k/ft}^2)(6 \text{ ft}) = \frac{2.40 \text{ k/ft}}{2.70 \text{ k/ft}}$$

Ans.

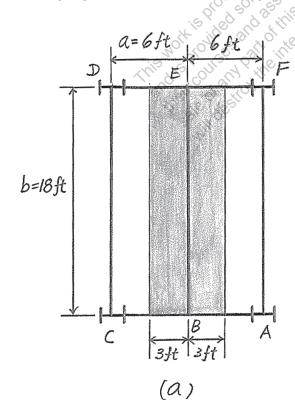
Due to symmetry, the vertical reactions at B and E are

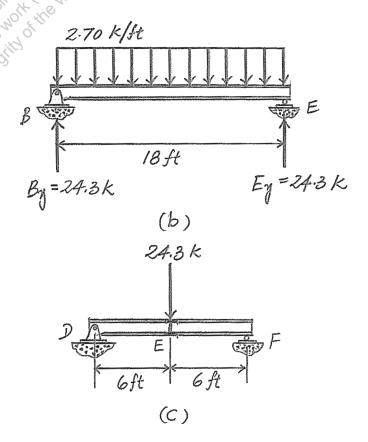
$$B_y = E_y = \frac{(2.70 \text{ k/ft})(18 \text{ ft})}{2} = 24.3 \text{ k}$$

The loading diagram of beam BE is shown in Fig. b.

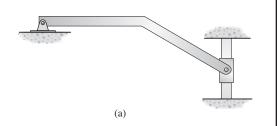
Beam FED. The only load this beam supports is the vertical reaction of beam BE at E, which is $E_v = 24.3$ k.

The loading diagram of beam *FED* is shown in Fig. c.



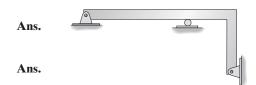


2–11. Classify each of the structures as statically determinate or indeterminate. If indeterminate, specify the degree of indeterminacy.

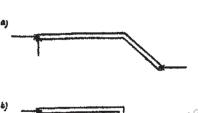


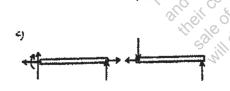
SOLUTION

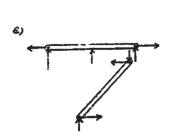
- (a) r = 33(1) = 3Statically determinate
- 3(1) < 5(b) r = 5Statically indeterminate to the second degree
- (c) r = 63(2) = 6Statically determinate
- (d) r = 103(3) < 10Statically indeterminate to the first degree
- (e) r = 7

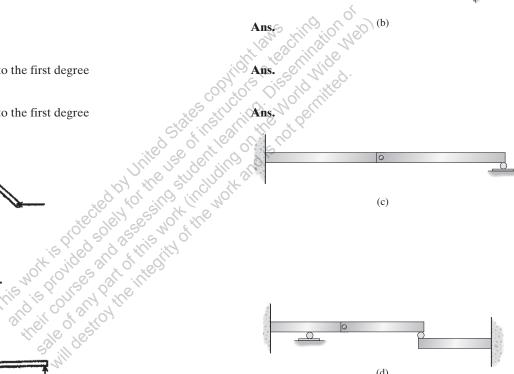


This work is protected by this estimation of the protection of the 3(2) < 7Their courses and assessing student learning of the work and the work and the intention of the work and the w Statically indeterminate to the first degree

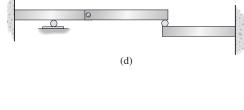


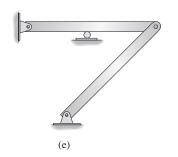


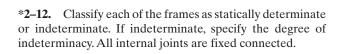


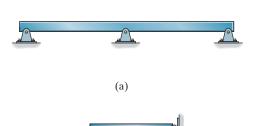


(c)









SOLUTION

$$r = 6$$
 $3n = 3(1) = 3$

$$r - 3n = 6 - 3 = 3$$

Stable and statically indeterminate to third degree.

$$r = 12$$
 $3n = 3(2) = 6$

$$r - 3n = 12 - 6 = 6$$

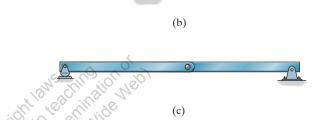
Stable and statically indeterminate to sixth degree.

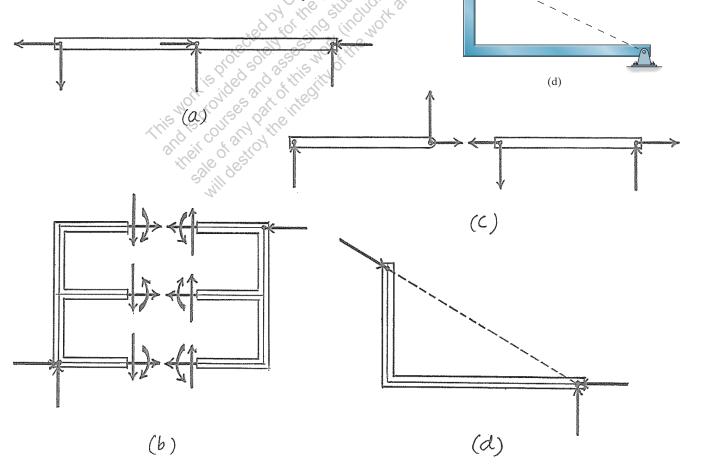
$$r = 5$$
 $3n = 3(2) = 6$

r < 3n

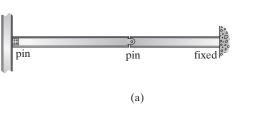
Unstable.

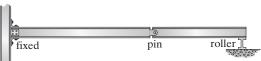
Unstable since the line of action of the reactive force components are concurrent.





2–13. Classify each of the structures as statically determinate, statically indeterminate, stable, or unstable. If indeterminate, specify the degree of indeterminacy. The supports or connections are to be assumed as stated.





(b)

(c)

SOLUTION

(a) r = 7 3n = 3(2) = 6 r - 3n = 7 - 6 = 1

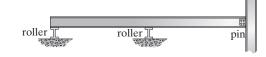
Stable and statically indeterminate to first degree.

(b) r = 6 3n = 3(2) = 6 r = 3n

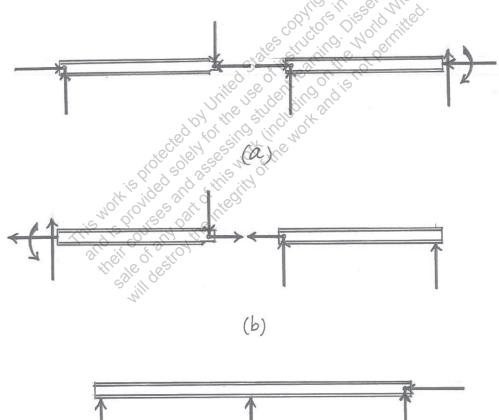
Stable and statically determinate

(c) r = 4 3n = 3(1) = 3 r - 3n = 4 - 3 = 1

Stable and statically indeterminate to first degree



pin



(C)

2–14. Classify each of the structures as statically determinate, statically indeterminate, stable, or unstable. If indeterminate, specify the degree of indeterminacy. The supports or connections are to be assumed as stated.

SOLUTION

(a) r = 53n = 3(2) = 6r < 3n

Unstable

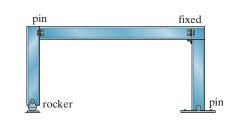
(b) r = 93n = 3(3) = 9r = 3n

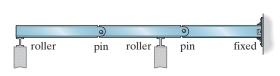
Stable and statically determinate

(c) r = 83n = 3(2) = 6

r - 3n = 8 - 6 = 2

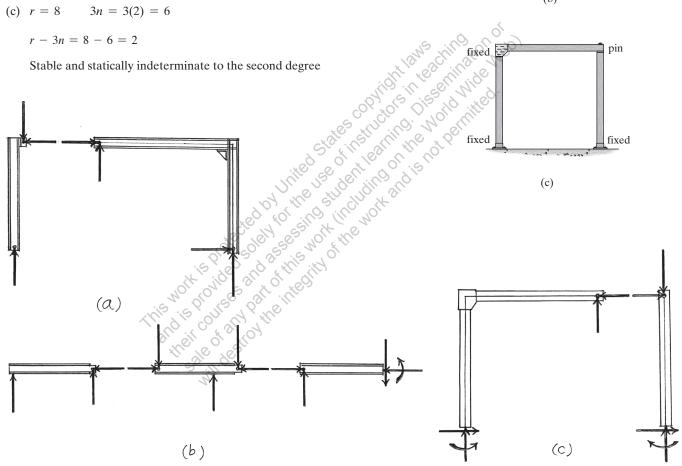
Stable and statically indeterminate to the second degree

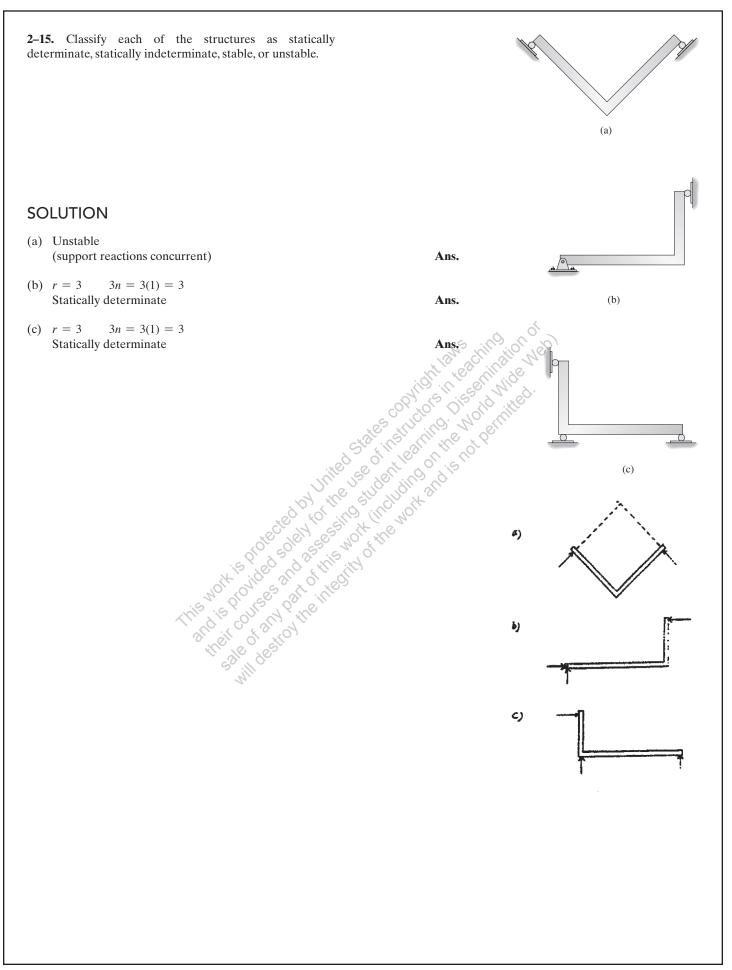




(b)

(a)





*2–16. Classify each of the structures as statically determinate, statically indeterminate, or unstable. If indeterminate, specify the degree of indeterminacy.

SOLUTION

(a) r = 6 3n = 3(1) = 3

$$r - 3n = 6 - 3 = 3$$

Stable and statically indeterminate to the third degree

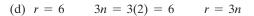
(b)
$$r = 4$$
 $3n = 3(1) = 3$

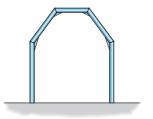
$$r - 3n = 4 - 3 = 1$$

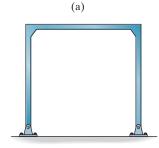
Stable and statically indeterminate to the first degree

(c)
$$r = 3$$
 $3n = 3(1) = 3$ $r = 3n$

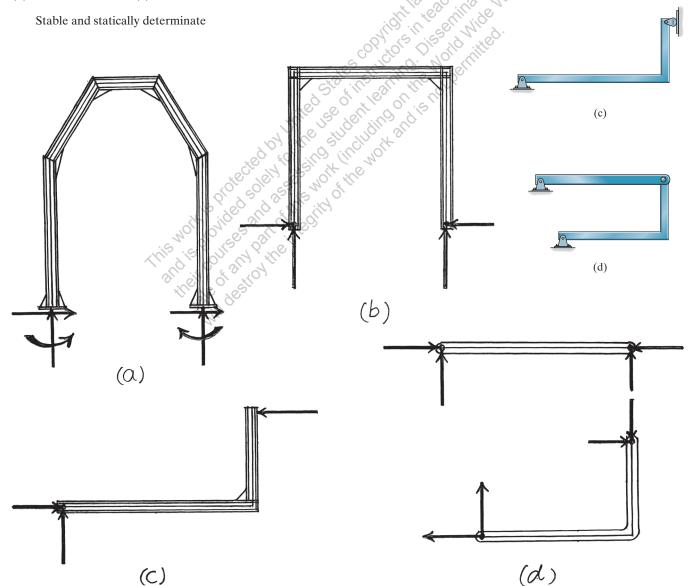
Stable and statically determinate

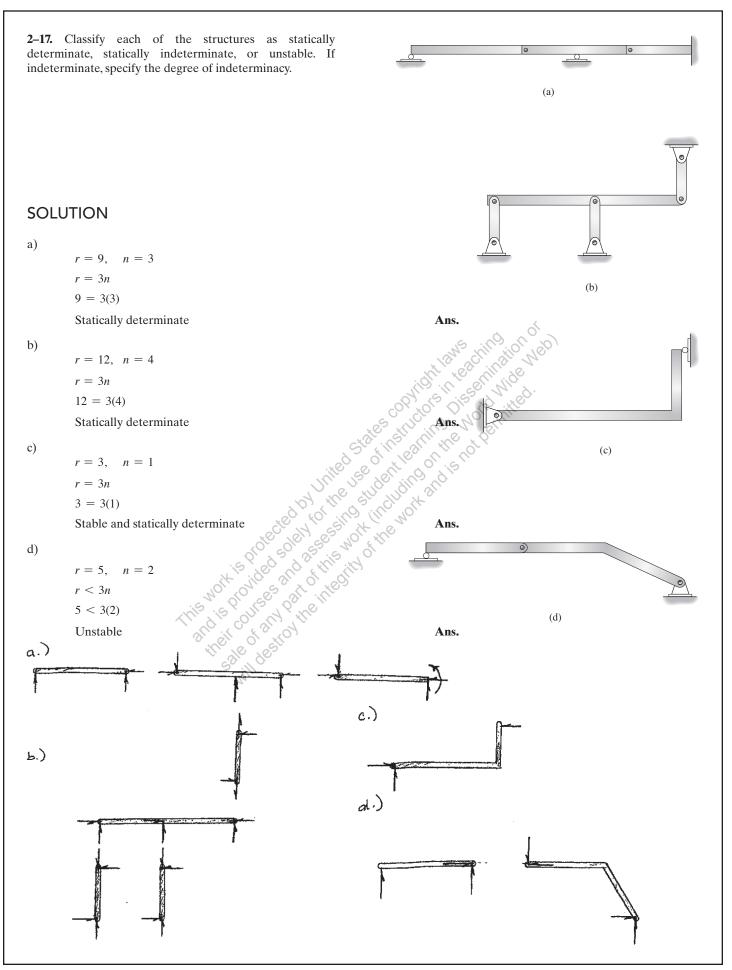




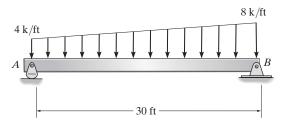


(b)





*2-18. Determine the reactions on the beam.



SOLUTION

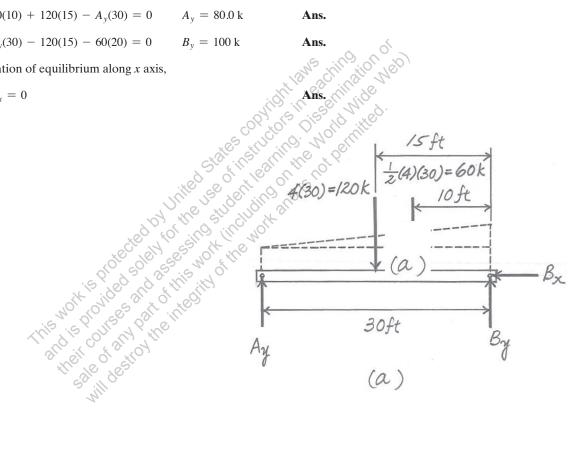
Equations of Equilibrium. Referring to the FBD of the beam in Fig. a, A_v and B_v can be determined directly by writing the moment equations of equilibrium about B and A respectively.

$$\zeta + \Sigma M_B = 0;$$
 $60(10) + 120(15) - A_v(30) = 0$ $A_v = 80.0 \text{ k}$

$$\zeta + \Sigma M_A = 0;$$
 $B_v(30) - 120(15) - 60(20) = 0$ $B_v = 100 \text{ k}$ Ans

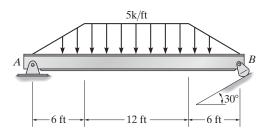
Write the force equation of equilibrium along x axis,

 $\pm \Sigma F_x = 0; \qquad B_x = 0$



Ans.

2–19. Determine the reactions at the supports.



SOLUTION

$$\zeta + \Sigma M_A = 0;$$
 $-15 \text{ k}(4 \text{ ft}) - 60 \text{ k}(12 \text{ ft}) - 15 \text{ k}(20 \text{ ft}) + F_B \cos 30^{\circ}(24 \text{ ft}) = 0$

$$F_B = 51.962 \,\mathrm{k} = 52.0 \,\mathrm{k}$$

Ans.

$$\stackrel{\pm}{\Rightarrow} \Sigma F_x = 0;$$

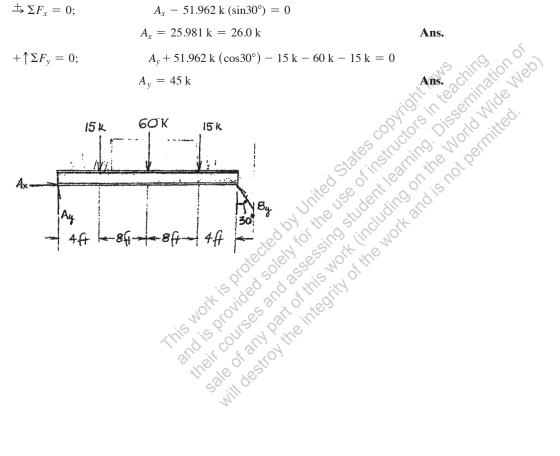
$$A_x - 51.962 \text{ k (sin}30^\circ) = 0$$

$$A_{\rm r} = 25.981 \,\mathrm{k} = 26.0 \,\mathrm{k}$$

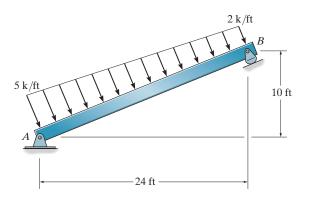
$$+\uparrow\Sigma F_{y}=0;$$

$$A_v + 51.962 \text{ k} (\cos 30^\circ) - 15 \text{ k} - 60 \text{ k} - 15 \text{ k} = 0$$

$$A_{v} = 45 \text{ k}$$



*2-20. Determine the reactions on the beam.



SOLUTION

$$\zeta + \Sigma M_A = 0;$$
 $F_B(26) - 52(13) - 39\left(\frac{1}{3}\right)(26) = 0$

$$F_B = 39.0 \text{ k}$$

$$+\uparrow \Sigma Fy = 0;$$
 $A_y - \frac{12}{13}(39) - \left(\frac{12}{13}\right)52 + \left(\frac{12}{13}\right)(39.0) = 0$

$$A_{\rm v} = 48.0 \, \rm k$$

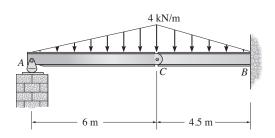
$$\pm \Sigma F_x = 0;$$
 $-A_x + \left(\frac{5}{13}\right) 39 + \left(\frac{5}{13}\right) 52 - \left(\frac{5}{13}\right) 39.0 = 0$

$$A_x = 20.0 \text{ k}$$

Ans.

= 0
Ans. Children Children

2–21. Determine the reactions at the supports *A* and *B* of the compound beam. There is a pin at C.



SOLUTION

Member *AC*:

$$\zeta + \Sigma M_C = 0; -A_v(6) + 12(2) = 0$$

$$A_{y} = 4.00 \text{ kN}$$

$$+\uparrow \Sigma F_{v} = 0; C_{v} + 4.00 - 12 = 0$$

$$C_{\rm v} = 8.00 \, {\rm kN}$$

$$+\Sigma F_x=0; C_x=0$$

Member *CB*:

$$\zeta + \Sigma M_B = 0; -M_B + 8.00(4.5) + 9(3) = 0$$

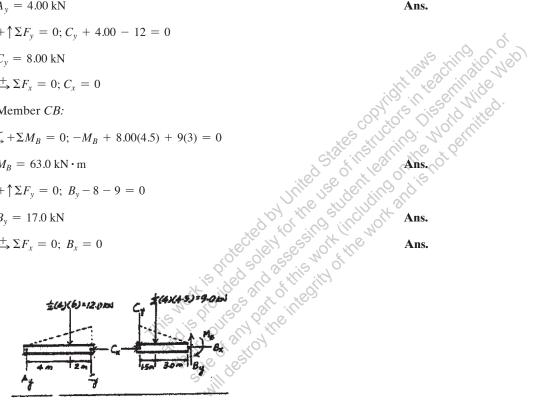
$$M_B = 63.0 \text{ kN} \cdot \text{m}$$

$$+\uparrow \Sigma F_{v} = 0; B_{v} - 8 - 9 = 0$$

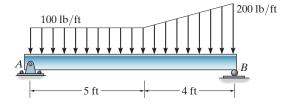
$$B_{\rm v} = 17.0 \, {\rm kN}$$

$$+\Sigma F_r=0; B_r=0$$

Ans.



2–22. Determine the reactions at the supports.



SOLUTION

$$\stackrel{+}{\longrightarrow} \Sigma F_x = 0; \quad A_x = 0$$

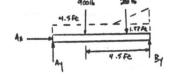
$$\zeta + \Sigma M_B = 0$$
; 900 (4.5) + 200 (1.333) - $A_y(9) = 0$

$$A_{y} = 480 \text{ lb}$$

$$+\uparrow \Sigma F_{y} = 0; 480 - 1100 + B_{y} = 0$$

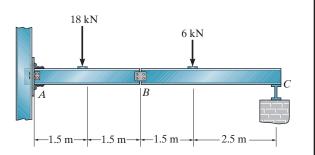
$$B_{\rm v} = 620 \, {\rm lb}$$

Ans.



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2–23. Determine the reactions at the supports A and C of the compound beam. Assume A is fixed, B is a pin, and C is a roller.



SOLUTION

Equations of Equilibrium. First consider the FBD of segment BC in Fig. a. N_C and B_{ν} can be determined directly by writing the moment equations of equilibrium about B and C respectively.

$$\zeta + \sum M_{\rm P} = 0$$
:

$$\zeta + \Sigma M_B = 0;$$
 $N_C(4) - 6(1.5) = 0$ $N_C = 2.25 \text{ kN}$
 $\zeta + \Sigma M_C = 0;$ $6(2.5) - B_y(4) = 0$ $B_y = 3.75 \text{ kN}$

$$N_C = 2.25 \text{ kN}$$

Ans.

$$\zeta + \sum M_{\alpha} = 0$$

$$6(2.5) - B_{\nu}(4) = 0$$

$$B_{\rm w} = 3.75 \, \rm kN$$

Ans.

Write the force equation of equilibrium along x axis,

$$\stackrel{+}{\Longrightarrow} \Sigma F_r = 0;$$

$$B_x = 0$$

Then consider the FBD of segment AB, Fig. b,

$$+$$
, $\Sigma F = 0$

$$4 = 0$$

$$\bot \uparrow \Sigma F = 0$$

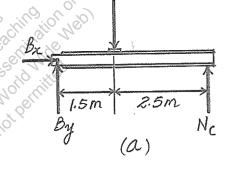
$$A_{\cdot \cdot \cdot} - 18 - 3.75 =$$

$$A_{v} = 21.75 \text{ kN}$$

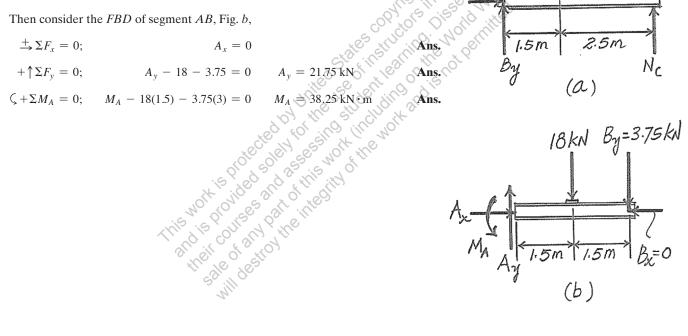
$$\zeta + \Sigma M_A = 0$$

$$M_A - 18(1.5) - 3.75(3) =$$

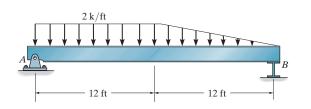
$$= 38.25 \,\mathrm{kN} \cdot \mathrm{m}$$



6KN



*2-24. Determine the reactions on the beam. The support at *B* can be assumed to be a roller.



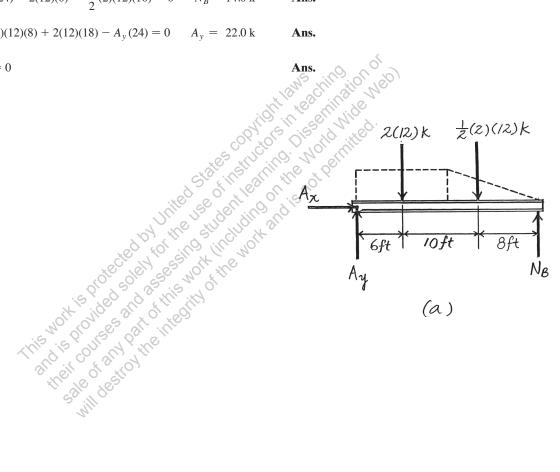
SOLUTION

Equations of Equilibrium:

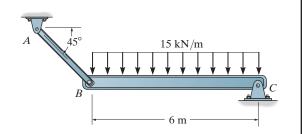
$$\zeta + \Sigma M_A = 0;$$
 $N_B(24) - 2(12)(6) - \frac{1}{2}(2)(12)(16) = 0$ $N_B = 14.0 \text{ k}$ Ans.

$$\zeta + \Sigma M_B = 0;$$
 $\frac{1}{2}(2)(12)(8) + 2(12)(18) - A_y(24) = 0$ $A_y = 22.0 \text{ k}$ Ans.

$$\stackrel{+}{\Longrightarrow} \Sigma F_x = 0; \qquad A_x = 0$$



2–25. Determine the horizontal and vertical components of reaction at the pins A and C.



SOLUTION

Equations of Equilibrium. Here, member AB is a two force member, which is reflected in the FBD of beam BC, Fig. a. F_{AB} and C_v can be determined directly by writing the moment equation of equilibrium about C and B respectively.

$$\zeta + \Sigma M_{\alpha} = 0$$

$$\zeta + \Sigma M_C = 0;$$
 $90(3) - F_{AB} \sin 45^{\circ} (6) = 0$ $F_{AB} = 63.64 \text{ kN}$ $\zeta + \Sigma M_B = 0;$ $C_y(6) - 90(3) = 0$ $C_y = 45.0 \text{ kN}$

$$F_{AB} = 63.64 \text{ kN}$$

$$\zeta + \Sigma M_{\rm B} = 0$$

$$C_{v}(6) - 90(3) = 0$$

$$C_{\rm v} = 45.0 \, \rm kN$$

Ans.

$$+\Sigma F = 0$$

$$C = 63.64 \cos 45^{\circ} = 0$$

$$C_{\rm r} = 45.0 \, {\rm kN}$$

$$+\Sigma F = 0$$

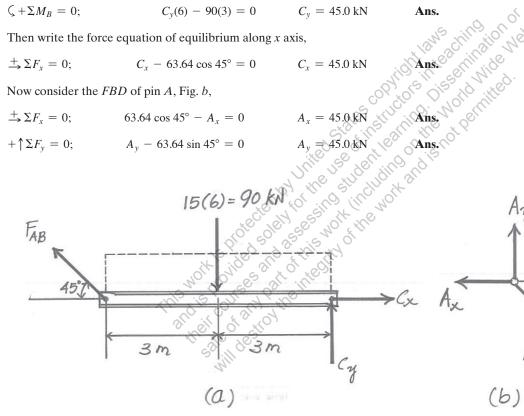
$$63.64 \cos 45^{\circ} - A_{r} = 0$$

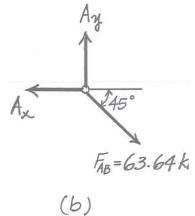
$$A_{..} = 45.0 \text{ kN}$$

$$+\uparrow\Sigma F_{\cdot\cdot}=0$$

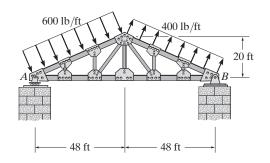
$$A_y - 63.64 \sin 45^\circ = 0$$

$$= 45.0 \,\mathrm{kN}$$





2-26. Determine the reactions at the truss supports A and B. The distributed loading is caused by wind.



SOLUTION

$$\zeta + \Sigma M_A = 0; \quad B_y(96) + \left(\frac{12}{13}\right) 20.8(72) - \left(\frac{5}{13}\right) 20.8(10) \\
- \left(\frac{12}{13}\right) 31.2(24) - \left(\frac{5}{13}\right) 31.2(10) = 0$$

$$B_y = 5.117 \, k = 5.12 \, k$$

$$+ \uparrow \Sigma F_y = 0; \quad A_y - 5.117 + \left(\frac{12}{13}\right) 20.8 - \left(\frac{12}{13}\right) 31.2 = 0$$

$$A_y = 14.7 \, k$$

$$\pm \Sigma F_x = 0; \quad -B_x + \left(\frac{5}{13}\right) 31.2 + \left(\frac{5}{13}\right) 20.8 = 0$$

$$B_x = 20.0 \, k$$
Ans.

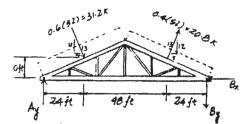
 $B_{y} = 5.117 \,\mathrm{k} = 5.12 \,\mathrm{k}$

$$+\uparrow \Sigma F_y = 0;$$
 $A_y - 5.117 + \left(\frac{12}{13}\right) 20.8 - \left(\frac{12}{13}\right) 31.2 = 0$

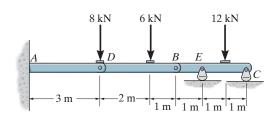
$$A_{v} = 14.7 \,\mathrm{k}$$

$$\pm \Sigma F_x = 0; \quad -B_x + \left(\frac{5}{13}\right) 31.2 + \left(\frac{5}{13}\right) 20.8 = 0$$

$$B_x = 20.0 \text{ k}$$



2–27. The compound beam is fixed at *A* and supported by a rocker at E and C. There are hinges (pins) at D and B. Determine the reactions at the supports.



SOLUTION

Equation of Equilibrium. First consider the *FBD* of segment *BD*, Fig. b.

$$\zeta + \Sigma M_D = 0;$$
 $B_y(3) - 6(2) = 0$ $B_y = 4.00 \text{ kN}$ $\zeta + \Sigma M_B = 0;$ $6(1) - D_y(3) = 0$ $D_y = 2.00 \text{ kN}$

$$B_{y} = 4.00 \text{ kN}$$

$$S(1) - D(3) = 0$$

$$D_{v} = 2.00 \text{ kN}$$

$$D_x - B_x = 0$$

$$\zeta + \Sigma M_C = 0$$
;

$$N_E = 12.0 \, \text{kN}$$

$$\zeta + \Sigma M_E = 0$$

$$N_C(2) + 4.00(1) - 12(1) = 0$$

$$N_C = 4.00 \, \text{kN}$$

$$B_{x}=0$$

$$D_{x} = 0$$

$$\xrightarrow{+} \Sigma F_r = 0;$$

$$A_r = 0$$

$$+ \uparrow \Sigma F_{v} = 0$$

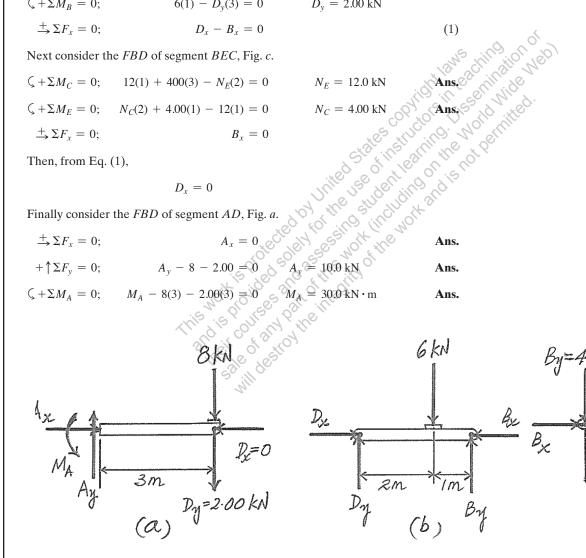
$$4 - 8 - 200 = 0$$

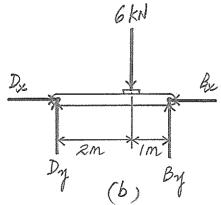
$$-8(3) - 200(3) = 0$$

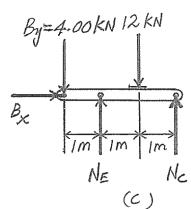


$$M_A - 8(3) - 2.00(3) = 0$$

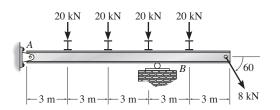
$$M_{\star} = 30.0 \,\mathrm{kN \cdot m}$$







*2-28. Determine the reactions on the beam. The support at B can be assumed as a roller.



SOLUTION

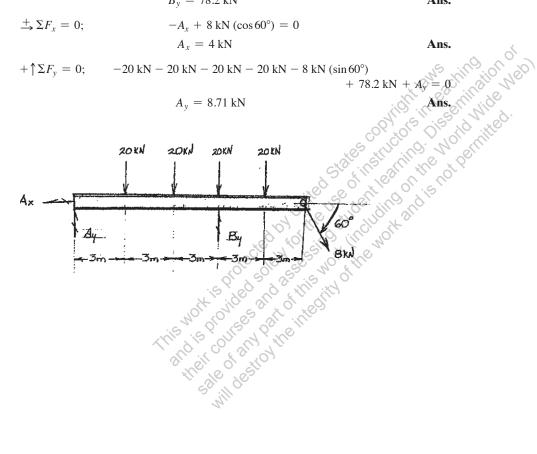
$$\zeta + \Sigma M_A = 0;$$
 $-20 \text{ kN}(3 \text{ m}) - 20 \text{ kN}(6 \text{ m}) - 20 \text{ kN}(9 \text{ m}) - 20 \text{ kN}(12 \text{ m}) - 8 \text{ kN}(\sin 60^\circ)(15 \text{ m}) + B_v(9 \text{ m}) = 0$

$$B_{\rm v} = 78.2 \, {\rm kN}$$
 Ans.

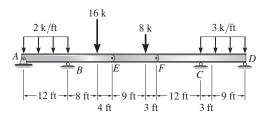
$$\stackrel{+}{\rightarrow} \Sigma F_x = 0;$$
 $-A_x + 8 \text{ kN } (\cos 60^\circ) = 0$

$$+\uparrow \Sigma F_v = 0;$$
 $-20 \text{ kN} - 20 \text{ kN} - 20 \text{ kN} - 8 \text{ kN} (\sin 60^\circ)$

$$+78.2 \text{ kN} + A_v = 0$$



2–29. Determine the reactions at the supports A, B, C, and D.



SOLUTION

Member EF:

$$\zeta + \Sigma M_F = 0$$
; 8 k(3 ft) $-E_v(12 \text{ ft}) = 0$

$$E_{\rm v} = 2 \, \rm k$$

$$+ \uparrow \Sigma F_{y} = 0$$
: $2 k - 8 k + F_{y} = 0$

$$F_{\rm v} = 6 \, \rm k$$

$$\zeta + \Sigma M_A = 0$$
; $-24 \text{ k}(6 \text{ ft}) + B_v(12 \text{ ft}) - 2 \text{ k}(24 \text{ ft}) = 0$

$$B_{\rm v} = 16 \, {\rm k}$$

$$+ \uparrow \Sigma F_{n} = 0$$
: $A_{n} - 24 k + 16 k - 2 k = 0$

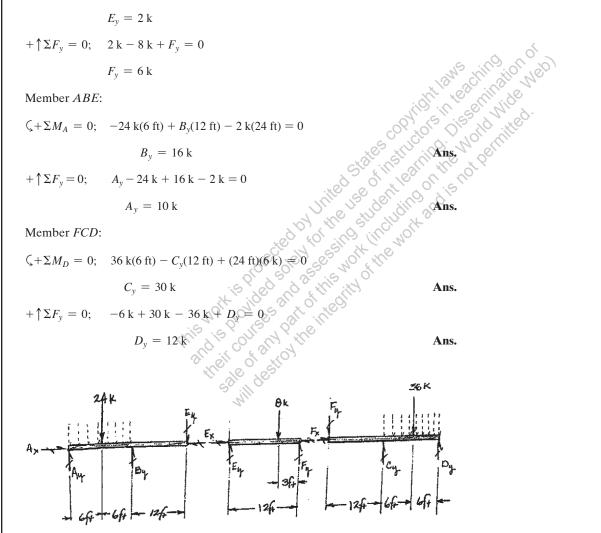
$$A_{v} = 10 \text{ k}$$

$$(+\Sigma M_p = 0)$$
 36 k(6 ft) - C (12 ft) + (24 ft)(6 k) = 0

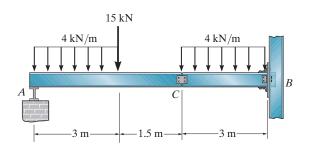
$$C_{\rm w} = 30 \, \rm k$$

$$+ \uparrow \Sigma F_{k} = 0$$
: $-6 k + 30 k - 36 k + D_{k} = 0$

$$D_{..} = 12 \, k$$



2–30. Determine the reactions at the supports A and B of the compound beam. Assume A is a roller, C is a pin, and B is fixed.



SOLUTION

Equations of Equilibrium. First consider the FBD of segment AC in Fig. a. N_A and C_{ν} can be determined directly by writing the moment equations of equilibrium about C and A respectively.

$$\zeta + \Sigma M_{\alpha} = 0$$

$$\zeta + \Sigma M_C = 0;$$
 $15(1.5) + 12(3) - N_A(4.5) = 0$ $N_A = 13.0 \text{ kN}$

$$N_A = 13.0 \, \text{kN}$$

$$\zeta + \Sigma M_{\star} = 0$$

$$\zeta + \Sigma M_A = 0;$$
 $C_v(4.5) - 12(1.5) - 15(3) = 0$ $C_v = 14.0 \text{ kN}$

$$C_{\rm v} = 14.0 \, \rm kN$$

Then write the force equation of equilibrium along x axis,

$$\xrightarrow{+} \Sigma F_x = 0;$$

$$C_x = 0$$

Now consider the FBD of segment CB, Fig. b,

$$+ \Sigma F_r = 0;$$

$$B_{x} = 0$$

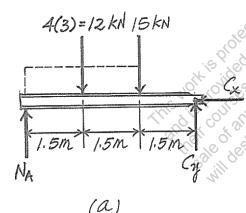
$$+\uparrow \Sigma F_{v}=0$$

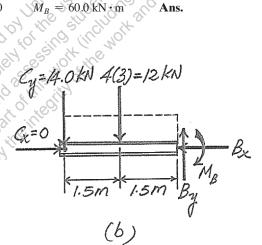
$$+\uparrow \Sigma F_{y} = 0;$$
 $B_{y} - 14.0 - 12 = 0$

$$\zeta + \Sigma M_{\pi} = 0$$

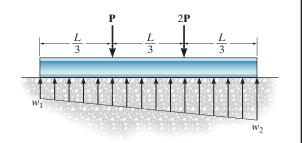
$$\zeta + \Sigma M_B = 0;$$
 $14.0(3) + 12(1.5) - M_B = 0$

$$= 60.0 \text{ kN} \cdot \text{m}$$
 Ans





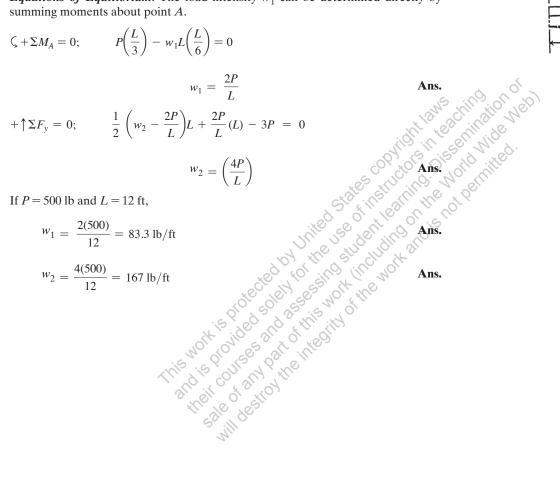
2–31. The beam is subjected to the two concentrated loads as shown. Assuming that the foundation exerts a linearly varying load distribution on its bottom, determine the load intensities w_1 and w_2 for equilibrium (a) in terms of the parameters shown; (b) set P = 500 lb, L = 12 ft.



SOLUTION

Equations of Equilibrium: The load intensity w_1 can be determined directly by summing moments about point A.

$$\zeta + \Sigma M_A = 0;$$
 $P\left(\frac{L}{3}\right) - w_1 L\left(\frac{L}{6}\right) = 0$

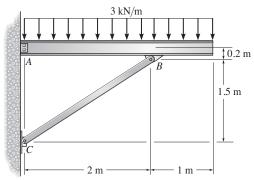


If P = 500 lb and L = 12 ft,

$$w_1 = \frac{2(500)}{12} = 83.3 \text{ lb/ft}$$

$$w_2 = \frac{4(500)}{12} = 167 \, \text{lb/ft}$$

*2-32. Determine the horizontal and vertical components of reaction at the supports A and C. Assume the members are pin connected at A, B, and C.



SOLUTION

$$\zeta + \Sigma M_A = 0; \left(\frac{3}{5}\right) F_{CB}(2) + \left(\frac{4}{5}\right) F_{CB}(0.2) - 9(1.5) = 0$$

$$F_{CB} = 9.926 \text{ kN}$$

$$\pm \Sigma F_x = 0; -A_x + \left(\frac{4}{5}\right) 9.926 = 0$$

$$A_B = 7.94 \text{ kN}$$

$$+\uparrow \Sigma F_y = 0; A_y + \frac{3}{5}(9.926) - 9 = 0$$

$$A_{v} = 3.04 \, \text{kN}$$

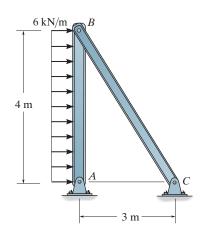
$$C_x = \frac{4}{5}(9.926) = 7.94 \,\text{kN}$$

$$C_y = \frac{3}{5}(9.926) = 5.96 \,\text{kN}$$





2-33. Determine the horizontal and vertical components of reaction at the supports A and C.



SOLUTION

Equations of Equilibrium. Member BC is a two force member, which is reflected in the FBD diagram of member AB, Fig. a. F_{BC} and A_x can be determined directly by writing the moment equations of equilibrium about A and B respectively.

$$\zeta + \Sigma M_A = 0$$

$$\zeta + \Sigma M_A = 0;$$
 $F_{BC} \left(\frac{3}{5}\right) (4) - 24(2) = 0$ $F_{BC} = 20.0 \text{ kN}$

$$F_{BC} = 20.0 \text{ kN}$$

$$\zeta + \Sigma M_B = 0;$$

$$24(2) - A_{*}(4) = 0$$

$$= 12.0 \text{ kN}$$

Write the force equation of equilibrium along y axis using the result of F_{BC} ,

$$+\uparrow\Sigma F_{v}=0;$$

$$20.0\left(\frac{4}{5}\right) - A_y = 0$$
 $A_y = 16.0 \text{ kN}$

$$A_{v} = 16.0 \, \text{kN}$$

Then consider the *FBD* of pin at *C*, Fig. *b*,

$$\xrightarrow{+} \Sigma F_r = 0$$

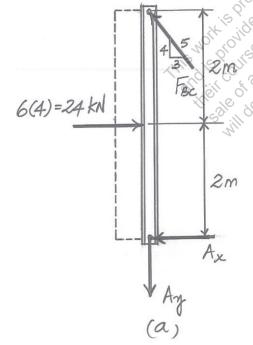
$$\stackrel{+}{\Rightarrow} \Sigma F_x = 0; \qquad 20.0 \left(\frac{3}{5}\right) - C_x = 0$$

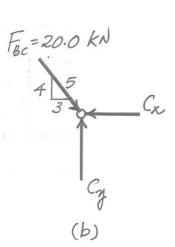
$$C_r = 12.0 \,\text{kN}$$

$$+\uparrow \Sigma F_{v}=0$$

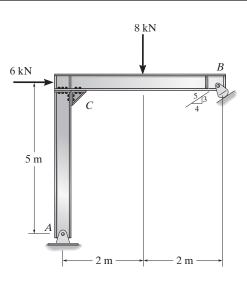
$$+\uparrow \Sigma F_y = 0;$$
 $C_y - 20.0\left(\frac{4}{5}\right) = 0$

$$= 16.0 \text{ kN}$$
 A





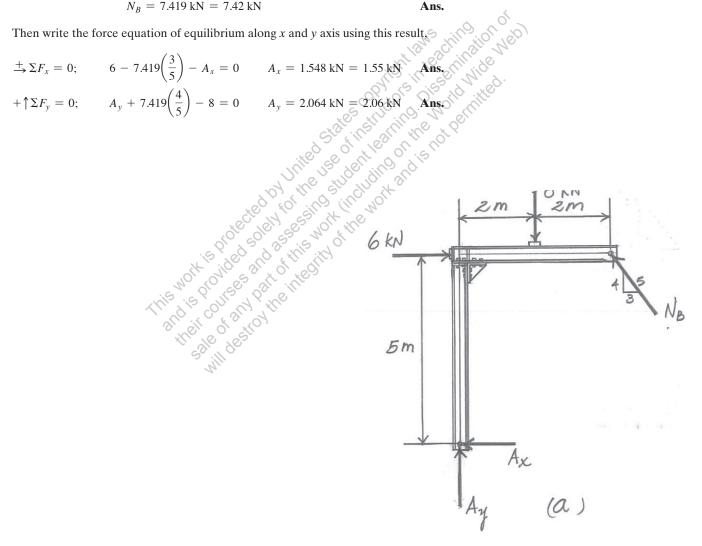
2-34. Determine the components of reaction at the supports. Joint C is a rigid connection.



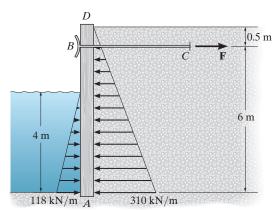
SOLUTION

Equations of Equilibrium. From the FBD of the frame in Fig. a, we notice that N_B can be determined directly by writing the moment equation of equilibrium about A.

$$\zeta + \Sigma M_A = 0;$$
 $N_B \left(\frac{3}{5}\right)(5) + N_B \left(\frac{4}{5}\right)(4) - 8(2) - 6(5) = 0$ $N_B = 7.419 \text{ kN} = 7.42 \text{ kN}$



2–35. The bulkhead AD is subjected to both water and soil-backfill pressures. Assuming AD is "pinned" to the ground at A, determine the horizontal and vertical reactions there and also the required tension in the ground anchor BC necessary for equilibrium. The bulkhead has a mass



SOLUTION

Equations of Equilibrium: The force in ground anchor BC can be obtained directly by summing moments about point A.

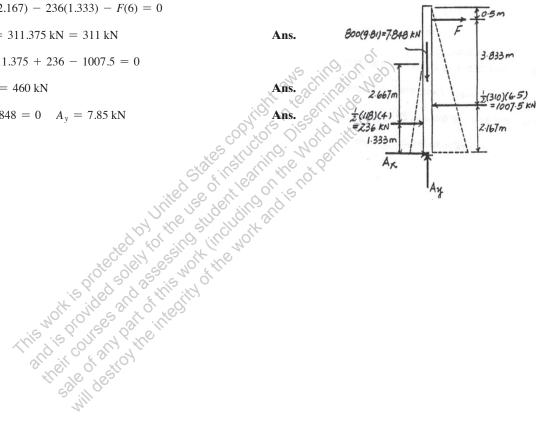
 $\zeta + \Sigma M_A = 0;$ 1007.5(2.167) - 236(1.333) - F(6) = 0

F = 311.375 kN = 311 kN

 $\xrightarrow{+} \Sigma F_r = 0;$ $A_r + 311.375 + 236 - 1007.5 = 0$

 $A_x = 460 \text{ kN}$

 $+\uparrow \Sigma F_{y} = 0;$ $A_{y} - 7.848 = 0$ $A_{y} = 7.85 \text{ kN}$



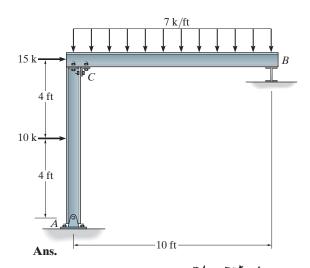
*2–36. Determine the reactions at the supports A and B. Assume the support at B is a roller. C is a fixed-connected joint.

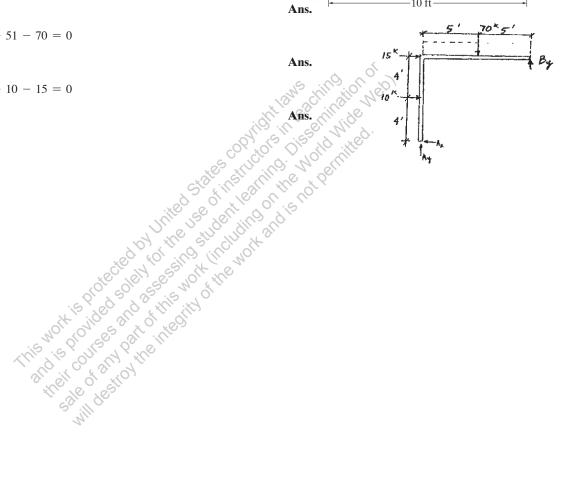
SOLUTION

$$+\Sigma M_A = 0;$$
 $B_y(10) - 70(5) - 10(4) - 15(8) = 0$ $B_y = 51 \text{ k}$ $+\uparrow \Sigma F_y = 0;$ $A_y + 51 - 70 = 0$

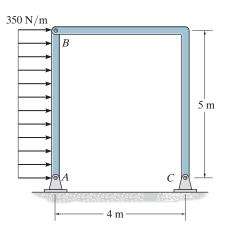
$$+ \leftarrow \Sigma F_x = 0;$$
 $A_x - 10 - 15 = 0$ $A_x = 25 \text{ k}$

 $A_{v} = 19 \, \text{k}$





2-37. Determine the horizontal and vertical reactions at A and C of the two-member frame.



SOLUTION

Equations of Equilibrium. Member BC is a two force member, which is reflected in the FBD of member AB, Fig a. \mathbf{F}_{BC} and \mathbf{A}_x can be determined directly by writing the moment equations of equilibrium about A and B respectively.

$$\zeta + \Sigma M_A = 0;$$
 $F_{BC} \left(\frac{4}{\sqrt{41}} \right) (5) - 1750(2.5) = 0$ $F_{BC} = 1400.68 \text{ N}$

$$\zeta + \Sigma M_R = 0;$$
 $1750(2.5) - A_r(5) = 0$

$$A_r = 875 \, \text{N}$$

$$+\uparrow \Sigma F_y = 0;$$
 $(1400.68) \left(\frac{5}{\sqrt{41}}\right) - A_y = 0$

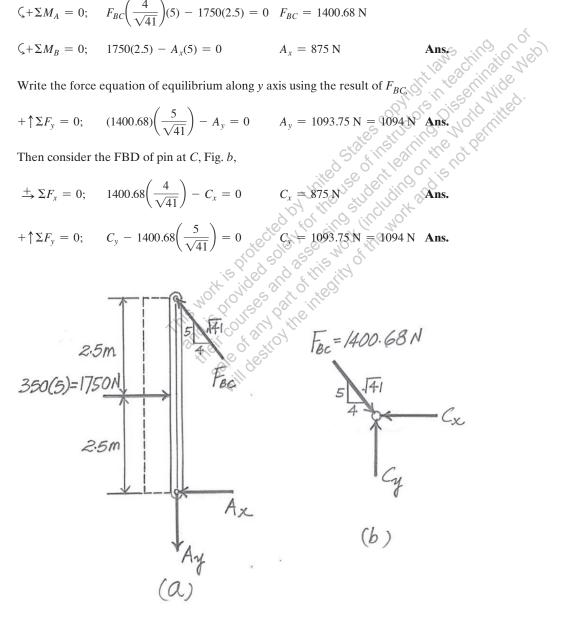
$$A_y = 1093.75 \text{ N} = 1094 \text{ N}$$
 An

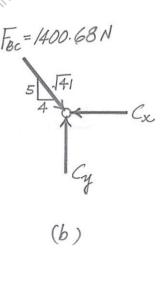
$$\stackrel{+}{\Longrightarrow} \Sigma F_x = 0;$$
 1400.68 $\left(\frac{4}{\sqrt{41}}\right) - C_x =$

$$C_x = 875 \,\mathrm{N}$$

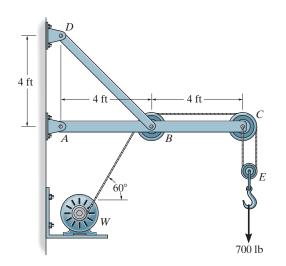
$$+\uparrow \Sigma F_y = 0;$$
 $C_y - 1400.68 \left(\frac{5}{\sqrt{41}}\right) = 0$

$$C_y = 1093.75 \,\mathrm{N} = 1094 \,\mathrm{N}$$
 Ans.





2–38. The wall crane supports a load of 700 lb. Determine the horizontal and vertical components of reaction at the pins A and D. Also, what is the force in the cable at the winch W?



SOLUTION

Pulley *E*:

$$+\uparrow \Sigma F_y = 0;$$
 $2T - 700 = 0$
 $T = 350 \text{ lb}$

Member *ABC*:

$$\zeta + \Sigma M_A = 0; \qquad T_{BD} \sin 45^\circ (4) - 350 \sin 60^\circ (4) - 700(8) = 0$$

$$T_{BD} = 2409 \text{ lb}$$

$$+ \uparrow \Sigma F_y = 0; \qquad A_y + 2409 \sin 45^\circ - 350 \sin 60^\circ - 700 = 0$$

$$A_y = 700 \text{ lb}$$

$$\pm \Sigma F_x = 0; \qquad A_x - 2409 \cos 45^\circ - 350 \cos 60^\circ + 350 - 350 = 0$$

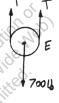
$$A_x = 1.88 \text{ k}$$
Ans.
$$D_x = 2409 \cos 45^\circ = 1703.1 \text{ lb} = 1.70 \text{ k}$$
Ans.
$$D_y = 2409 \sin 45^\circ = 1.70 \text{ k}$$
Ans.

$$+\uparrow \Sigma F_y = 0;$$
 $A_y + 2409 \sin 45^\circ - 350 \sin 60^\circ - 700 = 0$
$$A_y = 700 \text{ lb}$$

$$\pm \Sigma F_x = 0; \qquad A_x - 2409\cos 45^\circ - 350\cos 60^\circ + 350 - 350 = 0$$

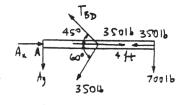
$$D_x = 2409 \cos 45^\circ = 1703.1 \text{ lb} = 1.70 \text{ k}$$

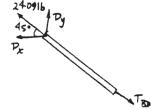
$$D_{\rm v} = 2409 \sin 45^{\circ} = 1.70 \,\rm k$$



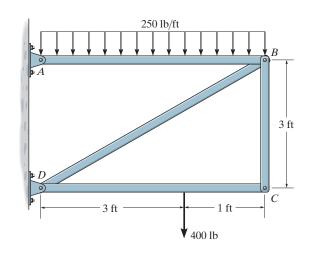
Ans.







2-39. Determine the horizontal and vertical force components that the pins support at A and D exert on the four-member frame.



SOLUTION

Equations of Equilibrium. First consider the FBD of member CD, Fig. a

$$\zeta + \Sigma M_D = 0;$$
 $F_{BC}(4) - 400(3) = 0$

$$F_{BC} = 300 \text{ lb}$$

$$\zeta + \Sigma M_B = 0;$$
 400(1) $-D'_y(4) = 0$ $D'_y = 100 \text{ lb}$

$$D_{y}' = 100 \text{ lb}$$

$$\xrightarrow{+} \Sigma F_x = 0;$$
 $D'_x = 0$

$$\zeta + \Sigma M_P = 0$$
: $1000(2) - A_0(4) = 0$

$$\pm \Sigma F_x = 0;$$
 1333.33 $\left(\frac{4}{5}\right) - A_x = 0$

$$A_x = 1066.67 \text{ lb} = 1067 \text{ lb}$$
 Ans,

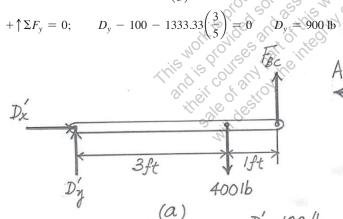
$$\pm \Sigma F_x = 0;$$
 $D_x - 1333.33 \left(\frac{4}{5}\right) = 0$

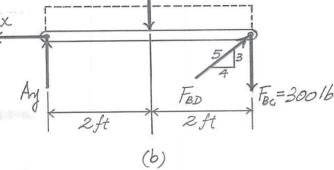
$$D_x = 1066.67 \, \text{lb} = 1067 \, \text{lb}$$
 Ans.

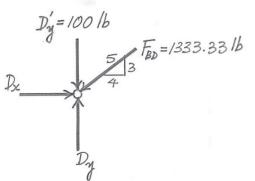
$$+\uparrow\Sigma F_{y}=0;$$

$$D_y - 100 - 1333.33 \left(\frac{3}{5}\right) = 0$$
 $D_y = 90$

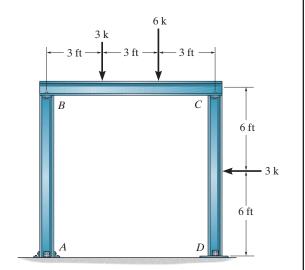
250(4)=1000 lb







*2–40. Determine the reactions at the supports A and D. Assume A is fixed and B, C and D are pins.



(1)

SOLUTION

Equations of Equilibrium. First consider the FBD of member BC, Fig. a

$$\zeta + \Sigma M_B = 0;$$
 $C_v(9) - 3(3) - 6(6) = 0$ $C_v = 5.00 \text{ k}$

$$\zeta + \Sigma M_C = 0;$$
 6(3) + 3(6) - $B_v(9) = 0$ $B_v = 4.00 \text{ k}$

$$+ \sum F_x = 0 \qquad B_x - C_x = 0$$

Then consider the FBD of member CD, Fig. b

$$\sum +\sum M_C = 0;$$
 $D_x(12) - 3(6) = 0$

$$D_x = 1.50 \,\mathrm{k}$$

$$\zeta + \Sigma M_D = 0$$
: $3(6) - C_2(12) = 0$

$$C_{\rm r} = 1.50 \, \rm k$$

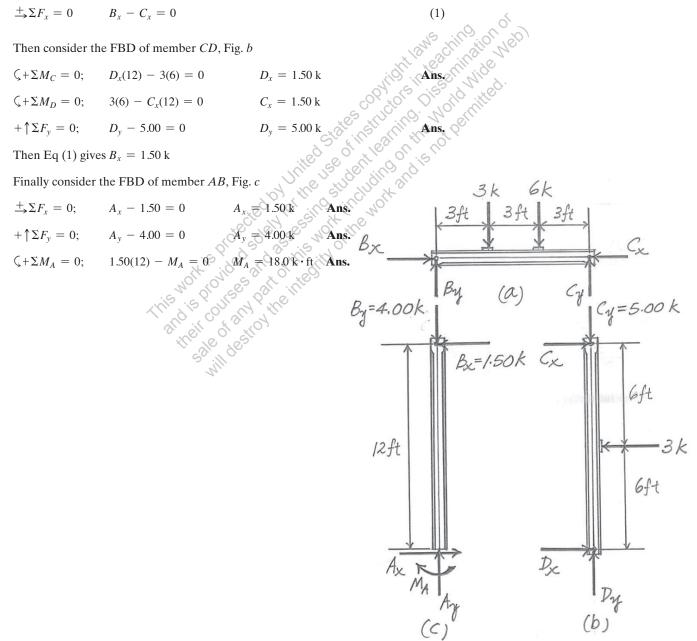
$$+\uparrow \Sigma F_{y} = 0$$
: $D_{y} - 5.00 =$

$$D_{v} = 5.00 \, \text{k}$$

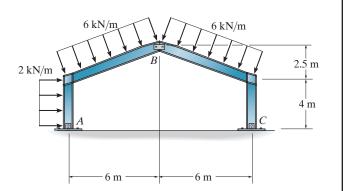
$$+\Sigma F_{x} = 0$$
: $A_{x} - 1.50 = 0$

$$+\uparrow \Sigma F_{v}=0;$$
 A_{v}

$$A_{v} - 4.00 = 0$$



2–41. Determine the components of reaction at the pinned supports A and C of the two-member frame. Neglect the thickness of the members. Assume B is a pin.



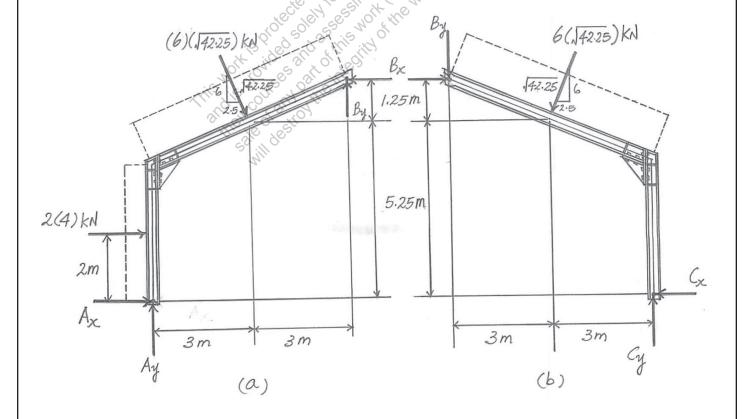
SOLUTION

Equations of Equilibrium. Referring to the FBD of members AB and BC shown in Fig. a and b, respectively, we notice that \mathbf{B}_x and \mathbf{B}_y can be determined by solving simultaneously the moment equations of equilibrium written about A and C, respectively.

$$\zeta + \Sigma M_A = 0; \quad B_x(6.5) + B_y(6) - (6) \left(\sqrt{42.25}\right) \left(\frac{2.5}{\sqrt{42.25}}\right) (5.25) \\
-(6) \left(\sqrt{42.25}\right) \left(\frac{6}{\sqrt{42.25}}\right) (3) - (2)(4)(2) = 0 \\
6.5B_x + 6B_y = 202.75$$

$$\zeta + \Sigma M_C = 0; \quad (6) \left(\sqrt{42.25}\right) \left(\frac{2.5}{\sqrt{42.25}}\right) (5.25) + (6) \left(\sqrt{42.25}\right) \left(\frac{6}{\sqrt{42.25}}\right) (3) \\
+ B_y(6) - B_x(6.5) = 0 \\
6.5B_x - 6B_y = 186.75$$

$$(2)$$



Ans.

2–41. (Continued)

Solving Eq (1) and (2) yields

$$B_x = 29.96 \,\mathrm{k}$$
 $B_y = 1.333 \,\mathrm{k}$

Using these results and writing the force equation of equilibrium by referring to the FBD of member AB, Fig. a,

$$^{+}\Sigma F_x = 0;$$
 $2(4) + (6)(\sqrt{42.25})(\frac{2.5}{\sqrt{42.25}}) - 29.96 + A_x = 0$

$$A_{\rm r} = 6.962 \,\mathrm{k} = 6.96 \,\mathrm{k}$$

$$+\uparrow \Sigma F_y = 0;$$
 $A_y + 1.333 - 6(\sqrt{42.25})(\frac{6}{\sqrt{42.25}}) = 0$

$$A_{\rm v} = 34.67 \,\mathrm{k} = 34.7 \,\mathrm{k}$$
 Ans.

$$\pm \Sigma F_x = 0;$$
 $29.96 - (6)(\sqrt{42.25})(\frac{2.5}{\sqrt{42.25}}) - C_x = 0$

$$C_{\rm r} = 14.96 \,\rm k = 15.0 \,\rm k$$

Referring to the FBD of member
$$BC$$
, Fig. b

$$\pm \Sigma F_x = 0; \qquad 29.96 - (6)\left(\sqrt{42.25}\right)\left(\frac{2.5}{\sqrt{42.25}}\right) - C_x = 0$$

$$C_x = 14.96 \text{ k} = 15.0 \text{ k}$$

$$+ \uparrow \Sigma F_y = 0; \qquad C_y - 1.333 - (6)\left(\sqrt{42.25}\right)\left(\frac{6}{\sqrt{42.25}}\right) = 0$$

$$C_y = 37.33 \text{ k} = 37.3 \text{ k}$$
Ans.

$$C_{\rm m} = 37.33 \,\mathrm{k} = 37.3 \,\mathrm{k}$$

2–42. Determine the horizontal and vertical components of reaction at A, C, and D. Assume the frame is pin connected at A, C, and D, and there is a fixed-connected joint at *B*.

50 kN 40 kN -1.5 m− 15 kN/m 4 m 6 m

SOLUTION

Member *CD*:

$$\zeta + \Sigma M_D = 0;$$
 $-C_x(6) + 90(3) = 0$
 $C_x = 45.0 \text{ kN}$

$$\stackrel{+}{\Longrightarrow} \Sigma F_x = 0; \quad D_x + 45 - 90 = 0$$

$$D_x = 45.0 \text{ kN}$$

$$+\uparrow \Sigma F_{v}=0;$$
 $D_{v}-C_{v}=0$

Member *ABC*:

$$D_{x} = 45.0 \text{ kN}$$

$$+ \uparrow \Sigma F_{y} = 0; \qquad D_{y} - C_{y} = 0$$

$$(1)$$
Member ABC :
$$\zeta + \Sigma M_{A} = 0; \qquad C_{y}(5) + 45.0(4) - 50(1.5) - 40(3.5) = 0$$

$$C_{y} = 7.00 \text{ kN}$$

$$+ \uparrow \Sigma F_{y} = 0; \qquad A_{y} + 7.00 - 50 - 40 = 0$$

$$A_{y} = 83.0 \text{ kN}$$

$$\Rightarrow \Sigma F_{x} = 0; \qquad A_{x} - 45.0 = 0$$

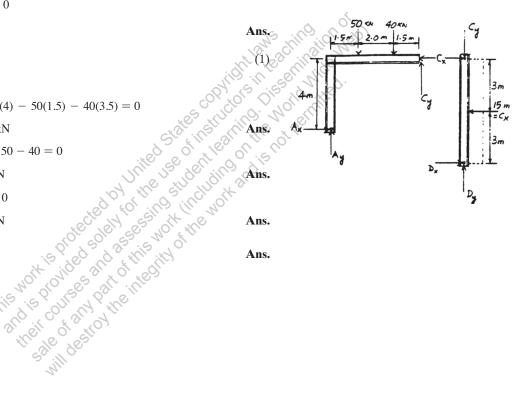
$$A_{x} = 45.0 \text{ kN}$$
From Eq. (1).
$$D_{y} = 7.00 \text{ kN}$$
Ans

$$+\uparrow \Sigma F_y = 0;$$
 $A_y + 7.00 - 50 - 40 = 0$
 $A_y = 83.0 \text{ kN}$

$$\pm \Sigma F_x = 0;$$
 $A_x - 45.0 = 0$ $A_x = 45.0 \text{ kN}$

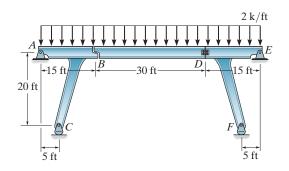
From Eq. (1).

$$D_{\rm v} = 7.00 \, {\rm kN}$$



Ans.

2-43. The bridge frame consists of three segments which can be considered pinned at A, D, and E, rocker supported at C and F, and roller supported at B. Determine the horizontal and vertical components of reaction at all these supports due to the loading shown.



SOLUTION

For segment *BD*:

$$\zeta + \Sigma M_D = 0;$$
 2(30)(15) - B_y (30) = 0 $B_y = 30 \text{ kip}$

$$\xrightarrow{+} \Sigma F_x = 0; \qquad D_x = 0$$

$$+\uparrow \Sigma F_{v} = 0;$$
 $D_{v} + 30 - 2(30) = 0$ $D_{v} = 30 \text{ kip}$

For segment *ABC*:

$$\zeta + \Sigma M_A = 0;$$
 $C_y(5) - 2(15)(7.5) - 30(15) = 0$ $C_y = 135 \text{ kip}$
 $\pm \Sigma F_x = 0;$ $A_x = 0$
 $+ \uparrow \Sigma F_y = 0;$ $-A_y + 135 - 2(15) - 30 = 0$ $A_y = 75 \text{ kip}$
For segment DEF :

$$\xrightarrow{+} \Sigma F_x = 0;$$
 $A_x = 0$

$$+\uparrow \Sigma F_{y} = 0$$
: $-A_{y} + 135 - 2(15) - 30 = 0$ $A_{y} = 75 \text{ kir}$

$$+\Sigma F = 0$$

$$+\uparrow \Sigma F_y = 0;$$
 $-E_y + 135 - 2(15) - 30 = 0$ $E_y = 75 \text{ kip}$





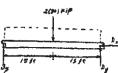




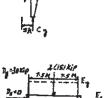


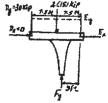




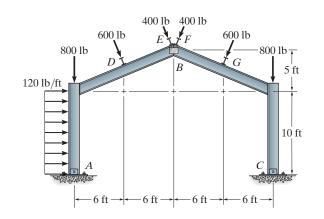








*2-44. Determine the horizontal and vertical reactions at the connections A and C of the gable frame. Assume that A, B, and C are pin connections. The purlin loads such as D and Eare applied perpendicular to the center line of each girder.



SOLUTION

Member *AB*:

$$\zeta + \Sigma M_A = 0;$$
 $B_x(15) + B_y(12) - (1200)(5) - 600 \left(\frac{12}{13}\right)(6) - 600 \left(\frac{5}{13}\right)(12.5)$ $-400 \left(\frac{12}{13}\right)(12) - 400 \left(\frac{5}{13}\right)(15) = 0$

$$B_{\nu}(15) + B_{\nu}(12) = 18,946.154$$

$$-400\left(\frac{12}{13}\right)(12) - 400\left(\frac{5}{13}\right)(15) = 0$$

$$B_x(15) + B_y(12) = 18,946.154$$
Member BC :
$$\zeta + \Sigma M_C = 0; \qquad -B_x(15) + B_y(12) + 600\left(\frac{12}{13}\right)(6) + 600\left(\frac{5}{13}\right)(12.5)$$

$$400\left(\frac{12}{13}\right)(12) + 400\left(\frac{5}{13}\right)(15) = 0$$

$$B_x(15) - B_y(12) = 12,446.15$$
Solving Eqs. (1) and (2),
$$B_x = 1063.08 \text{ lb.}$$

$$B_y = 250.0 \text{ lb}$$
Member AB :
$$\Delta \Sigma F_x = 0; \qquad -A_x + 1200 + 1000\left(\frac{5}{13}\right) - 1063.08 = 0$$

$$A_x = 522 \text{ lb}$$
Ans.
$$+ \uparrow \Sigma F_y = 0; \qquad A_y - 800 - 1000\left(\frac{12}{13}\right) + 250 = 0$$

$$A_x = 1473 \text{ lb}$$
Ans.

$$15) - B_{\nu}(12) = 12,446.15$$

$$B_{\rm x} = 1063.08 \, \text{lb}.$$
 $B_{\rm y} = 250.0 \, \text{lb}$

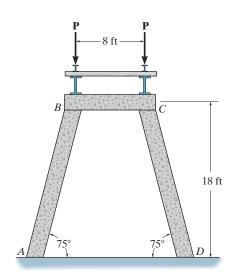
$$+\uparrow \Sigma F_y = 0;$$
 $A_y - 800 - 1000 \left(\frac{12}{13}\right) + 250 = 0$

$$A_{y} = 1473 \text{ lb}$$
 Ans.

Member *BC*:

$$+\uparrow \Sigma F_y = 0;$$
 $C_y - 800 - 1000 \left(\frac{12}{13}\right) - 250.0 = 0$ $C_y = 1973 \text{ lb}$

2-1P. The railroad trestle bridge shown in the photo is supported by reinforced concrete bents. Assume the two simply supported side girders, track bed, and two rails have a weight of 0.5 k/ft and the load imposed by a train is 7.2 k/ft. Each girder is 20 ft long. Apply the load over the entire bridge and determine the compressive force in the columns of each bent. For the analysis assume all joints are pin connected and neglect the weight of the bent. Are these realistic assumptions?



SOLUTION

Maximum reactions occur when the live load is over the entire span.

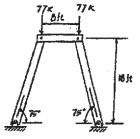
Load =
$$7.2 + 0.5 = 7.7 \, \text{k/ft}$$

$$R = 7.7(10) = 77 \text{ k}$$

Then
$$P = \frac{2(77)}{2} = 77 \text{ k}$$

$$\zeta + \Sigma M_B = 0; -77(8) + F \sin 75^{\circ}(8) = 0$$

$$F = 79.7 \, \text{k}$$



It is not reasonable to assume the members are pin connected, since such a framework is unstable.

Ans.

